A New Index for Detecting Frequency of Unknown Underwater Weak Signals with Genetic Algorithm

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Abstract—In this paper, a new index is proposed for detecting the frequency of unknown underwater signals based on the stochastic resonance theory. When the received weak signal is input into the stochastic resonance system, first, by frequency analysis, the frequency with the highest amplitude A_m of the output signal spectrum is considered as the pre-detection frequency. Then a cosine signal with the pre-detection frequency and unit amplitude is constructed. Define the pre-signal-to-noiseratio as the logarithm of the squared amplitude A_m over the mean of signal amplitudes in all other frequencies. The new index is defined as the product of the pre-signal-to-noise-ratio and the correlation coefficient between the received unknown signal and the constructed cosine signal. The new index is featured by taking into account the signal characteristics in both time and frequency domain, and it will yield better signal frequency detection performance. In addition, to improve the time efficiency of the frequency detection, a method to bound the searching range, keyed to the genetic algorithm, of the stochastic resonance system parameters is proposed. The method can be used to detect the frequency of both single frequency and frequency-hopping unknown signals. With the designed new index and system parameter bounding method, the simulations and experiments for the weak underwater unknown signals are conducted. Compared to the piecewise mean value index and weighted power spectral kurtosis index, the new index yields a higher detection probability at varied input signal-to-noise ratios and signal frequencies. With bounding system parameter searching ranges, the time efficiency is improved. The main purpose of this paper is to detect the frequency of unknown underwater weak signals by stochastic resonance system with genetic algorithm. The main contributions are summarized as follows. First, the detection probability of weak signals is improved by stochastic resonance system with the proposed signal detection index than some other indexes. Second, to improve the time efficiency of the signal frequency detection, a method to bound the searching range of system parameters is proposed.

Keywords—Stochastic resonance; underwater weak signal detection; genetic algorithm; frequency detection; frequency-hopping signal; index

I. INTRODUCTION

The detection and identification of underwater unknown targets are of great significance for the coastal defense development. However, because of natural and human activities, the underwater environment is very complex, such as wind and waves on the sea surface, marine biological activities, ocean currents on the seabed and the movement of hulls. In addition, some underwater targets can change their frequencies and other information to hide themselves. These factors make the detection and identification of underwater targets more challenging. Therefore, the efficient detection of underwater targets in such a complex environment is very important for both scientific research and engineering practice. The methods of traditional weak signal detection usually use finite impulse response (FIR) and infinite impulse response (IIR) [1], [2] filters to filter out the background noise mixed with the signal. Although these methods have some effects on filtering the out-of-band noise of signal, they will fail when the noise is distributed in the signal band. Stochastic resonance (SR) [3] theory is a weak signal detection method with high efficiency, which is different from traditional signal detection methods. With the SR system, the weak signal can be enhanced, and the system output signal-to-noise ratio (SNR_o) will be maximized by utilizing the background noise. The SR system is mainly composed of weak signal, background noise, and nonlinear system [4]. SR theory was first proposed by R.Benzi et al. in 1981 [5], which explained a phenomenon that the glacial and warm climates occurred periodically in ancient climate. Then SR theory has been further developed. Nowadays, it has been applied extensively to many subjects such as meteorology [6], hydroacoustics [7], biomedicine [8] and mechanical mechanics [9], [10].

In recent years, researchers have paid more attention to the field of weak signal detection based on SR theory. Wang et al. The author in [11] extend the bistable SR system to the tri-stable system by adjusting the three potential heights of SR system potential function. They use the differential evolutionary particle swarm algorithm to search the optimal values of system parameters, which can effectively improve the system SNR_o by simulations and experiments. Zheng *et al.* The author in [12] propose a fractional-order stochastic resonance (FOSR) multi-parameter optimization algorithm based on genetic algorithm (GA), which is beneficial to the application and popularization of FOSR in weak signal detection. H. T. Reda et al. The author in [13] discuss the application of SR in spectrum sensing and propose a firefly-inspired algorithm to optimize the SR and noise parameters of the dynamic system to improve signal detection. Guo et al. [14], [15] detect the multi-frequency weak signal by the cascading and paralleling of SR system. Based on the adiabatic approximation theory [16], SR theory is applicable to the signal detection of low frequency («1Hz). However, most of the signal frequencies in practical applications are not low. Leng et al. The authors in [17], [18] propose to transform high frequency to low frequency signals by using scale transformation and secondary sampling theory such that the high frequency weak signals can be detected based on SR theory. Ji et al. [19] realize the detection of hydroacoustic high frequency chirp signals by SR system, and verify the correctness and feasibility of this method by simulations and experiments. The performance of SR system is directly related to the detection probability of weak signal. It is crucial to design a index with high adaptability for weak signal detection, which can keep the resonance response to follow the unknown signal features. The SNR_o can be increased by SR system, hence SNR_o and signalto-noise ratio gain (SNR_g) [20], [21] are the most common and intuitive indexes for measuring the performance of the adaptive SR system. However, to calculate SNR_o and SNR_a , some prior information should be available, such as the frequency of weak signal. Normally, these prior information cannot be obtained in practical applications. It is indispensable to define a new index for the detection of completely unknown signals. Therefore, many new indexes have been proposed, such as weighted kurtosis index [22], time domain correlated kurtosis index [23], correlation coefficient index [24], weighted power spectrum kurtosis (WPSK) index [25], entropy kurtosis variation product index [26] and piecewise mean value index (PMV) [27]. Although these indexes are feasible in some conditions, their adaptability is constrained. For example, for some single indexes, the time and frequency domain characteristics of the signal cannot be taken together to detect the signal. For some multiple indexes, they are sensitive to signal frequency and pulse signal. When the input signal frequency is high or the input signal contains a large amount of pulse signals, with these indexes the weak signal detection probability is low. In this paper, a new index is proposed to improve the weak signal detection probability by SR system.

The contributions of this paper are as follows. First, a new index is designed for weak signal detection and GA is used as the optimization method to search the optimal values of system parameters. The signal detection probability with the new index is proved to be higher than that by SR systems with PMV and WPSK indexes through simulations and experiments. The designed new index takes into account both the time and frequency domain characteristics of the signal, and it is insensitive to the change of signal frequency. Second, to decrease the frequency detection time for both single frequency and frequency-hopping signals, a method to bound the searching ranges of system parameters is proposed. However, there are some limitations in the existing work. The experimental site is located at the seaside of Xing-hai Park in Dalian City in this paper, which is different from the deep sea. In addition, the simulation is carried out in Gaussian noise, which is different from the actual noise type.

The remaining parts of this paper are organized as follows. The SR theory and the definition of a new index are introduced in Section II. For single frequency and frequency-hopping signals, the method to bound the searching ranges of system parameters a and b is presented in Section III. The simulations and experiments are analyzed in Section IV and V. The results and discussion are introduced in Section VI. The future plans and improvements are introduced in Section VII. Finally, this paper is concluded in Section VIII.

II. NEW INDEX DEFINITION AND DESIGN OF SR SYSTEM

A. Stochastic Resonance Theory

The bistable SR system can be given by nonlinear Langevin equation [28],

$$\frac{dx}{dt} = -V'(x) + s(t) + n(t) \tag{1}$$



Fig. 1. The Potential Function Curve of V(x), when a = b = 1. ΔV is the Potential Height, x_m is the Half Width of Potential well, $\tan \theta = \Delta V/x_m$.



Fig. 2. The Curve of SNR_o with Noise Intensity D, when A = 0.1, a = b = 1.

where $V(x) = -\frac{a}{2}x^2 + \frac{b}{4}x^4$ is the potential function and its curve is shown in Fig. 1. x is the SR system output signal. System parameters a and b are real numbers greater than zero. $s(t) = A\cos(2\pi f_0 t)$ is the weak periodic signal to be detected, A is the signal amplitude and f_0 is the frequency. n(t) is the noise, and $n(t) = \sqrt{2D\varepsilon}(t)$. D is the noise intensity and $\varepsilon(t)$ represents the Gaussian white noise with zero mean and variance one.

The SR system is in a stable state and the particle is in one of the two potential wells when there is no external signal input to the system. When an appropriate noise is input to the system, the particle will obtain energy from the noise and then skip the potential barrier to complete the transition between the two potential wells. Because the voltage difference between the two bistable potential wells is much larger than the original input signal amplitude, the SNR_o of SR system is greatly improved in this situation. The SNR_o of SR system is given by

$$SNR_o \approx \sqrt{2}\Delta V \left(\frac{A}{D}\right)^2 e^{-\frac{\Delta V}{D}}$$
 (2)

where A is the amplitude of system input signal s(t), ΔV is the potential height of the potential function. The SNR_o with respect to the noise intensity D is shown in Fig. 2.

It is inefficient and lacks of adaptivity to put the nonlinear system in a resonant state by adjusting noise intensity [29]. The potential height ΔV determined by the system parameters a and b is crucial for the particle to complete the periodic transition between the two potential wells. Parameters a and b can be searched by some optimization methods. In this paper, we choose GA as the optimization method to search

the optimal values of system parameters dynamically [30].

To detect the signal frequency by SR system, it is required that the input signal be of low frequency. A signal with high frequency can be down-converted into a low frequency signal by re-sampling the original signal with a ratio R. Then the low frequency f'_0 of weak signal can be detected by SR system and finally we can restore the actual signal frequency by $f_0 = f'_0 \times R$.

B. Definition of the New Index

For the frequency detection of unknown signals, various indexes have been proposed such as PMV and WPSK indexes. However, the signal frequency detection probability with these indexes are low. Herein, we propose a new index for the signal frequency detection through a SR system. Denote the received unknown weak signal by r(t) and r(k) is its sampled one signal. The new index is designed as follows.

I). The output signal x(k) of SR system can be calculated by the fourth-order Longe-Kutta algorithm. The Fourier transform of x(k) is denoted by H(f). The frequency with the maximum amplitude of H(f) is denoted by f_m .

II). Construct a new cosine signal $s'(t) = \cos(2\pi f_m t)$ with frequency f_m and initial phase zero. The absolute value of the correlation coefficient between r(t) and s'(t) is written as C = |R(r(k), s'(k))|, where r(k) and s'(k) are the sampling signals of r(t) and s'(t), respectively.

III). The pre-signal-to-noise ratio of the output signal x(k) is defined as $PSNR = 10 \times \log_{10} \frac{H^2(f_m)}{\sum_{f \neq f_m} H(f)/N}$, where $H(f_m)$ is the peak amplitude of H(f) and N is the length of output signal x(k).

IV). The new index, called CSNR, is defined as the product of C and PSNR, and the value of CSNR can be calculated by $\gamma_{csnr} = C \times PSNR$, which will be used as the fitness function of GA for searching the optimal values of system parameters a and b.

C. Process Detecting the Frequency of Weak Signals with the New Index

The sampled signal r(k) of received unknown weak signal r(t) is input to the optimal SR system and its spectrum H(f) is obtained. The frequency with the maximum spectrum amplitude is considered as the frequency of r(t). The frequency detecting process of the optimal SR system for detecting the frequency of weak signals is shown in Fig. 3.



Fig. 3. The Frequency Detecting Process of SR System.

When the frequency with the maximum spectrum amplitude is not the target signal frequency f_0 , s'(t) and r(t)will not be highly correlated, and the value of C will be smaller. Hence, C can be used as a single time domain index. In addition, when the value of PSNR is larger, the peak amplitude of output signal spectrum is larger than other amplitudes obviously, which can reduce the influence of other random frequencies on the frequency with the maximum spectrum amplitude. Hence, the value of PSNR can be used as a single frequency domain index. To jointly consider both the time and frequency domain characteristics of the output signal, the product of the two single indexes can be a new index, which will yield better detection performance. When n(t) is zero mean Gaussian noise, the correlation coefficient between r(t) and s'(t) is

$$C = |R(r(k), s'(k))| = \frac{|Cov(r(k), s'(k))|}{\sqrt{Var(r(k)) \times Var(s'(k))}}$$
(3)

The denominator of (3) is a constant and its numerator is

$$c = \left| \sum_{k=1}^{N} s(k) \times s'(k) + \sum_{k=1}^{N} n(k) \times s'(k) \right|$$

$$= \begin{cases} c_1, f_m = f_0 \\ c_2, f_m \neq f_0 \end{cases}$$
(4)

Generally, $c_1 \ge c_2$, where c is the numerator of (3), s(k), s'(k) and n(k) are the sampled signal of s(t), s'(t) and n(t), respectively. N is the number of signal s(k). When $f_m = f_0$, $c = c_1$, otherwise, $c = c_2$.

III. A METHOD TO BOUND THE SEARCHING RANGES OF SYSTEM PARAMETERS a and b

A. The Searching Range of System Parameter b for Single Frequency Signal Detection

The intensity of noise added to the nonlinear system will affect SR system operation. If the noise intensity is too low, the particle cannot obtain enough energy from the noise to skip the potential barrier. If the noise intensity is too high, although the particle can obtain enough energy from the noise to skip the potential barrier and resonance will occur, there will be a large amount of random noise mixed with the output signal. In this situation, the SNR_o of SR system is still very low and the signal frequency cannot be detected from the output signal with the strong background noise. Different potential heights ΔV determined by system parameters a and b have different fitness values of GA. The optimal values of system parameters a and b can be obtained by GA with the CSNR index. To reduce the searching time of system parameters a and b, we propose a method to limit the searching range of parameter b for GA.

From Fig. 1, the half width of potential well $x_m = \sqrt{\frac{a}{b}}$ and the potential height $\Delta V = \frac{a^2}{4b}$ [31]. The critical conditions for the particle to skip the potential barrier are given by

$$\begin{cases} \frac{\partial V(x,t)}{\partial x} = -ax + bx^3 = 0\\ \frac{\partial^2 V(x,t)}{\partial x^2} = -a + 3bx^2 = 0 \end{cases}$$
(5)

Where x is the system output signal. Hence, the critical amplitude of particle is $A_c = \sqrt{\frac{4a^3}{27b}}$, which is considered as the threshold for the particle to skip the potential barrier. The amplitude of signal and noise intensity need to satisfy

$$\begin{cases}
A \le A_c \\
A_c \le A + D
\end{cases}$$
(6)

When A > D, the input signal-to-noise ratio (SNR_i) of system is high, and we can obtain the signal frequency from the received signal spectrum easily. Hence, assume $A \leq D$, from (6), we can obtain $b \geq \frac{4a^3}{27(A+D)^2} \geq \frac{4a^3}{27(2D)^2}$, where A is the amplitude of input signal s(t), and D is the noise intensity. When the standard deviation of noise n(t) is $\sqrt{2D}$, hence, we can obtain the received signal power $P \approx 2D$. Therefore, $b \geq \frac{4a^3}{27P^2}$ at low SNR_i , which indicates the potential height ΔV determined by the system parameters a and b would not be large. In addition, ΔV would not be small, otherwise, there will be a large amount of random noise mixed with the output signal. In this situation, the frequency f_0 of the target signal cannot be distinguished from other random frequencies. Hence, we can set a searching range for the parameter b. Define $\tan \theta = \frac{\Delta V}{x_m} = \frac{a\sqrt{a}}{4\sqrt{b}}$ (see Fig. 1 for θ). Therefore, we can obtain the searching range of parameter b, where P is the power of the received signal

$$\frac{4a^3}{27P^2} \le b \le \frac{a^3}{16\left(\tan\theta\right)^2}$$
(7)

B. The Searching Ranges of System Parameters a and b for Frequency-Hopping Signal Detection

To detect the frequency of frequency-hopping signal by the proposed SR system and reduce the searching time of parameters a and b, we will constrain the searching ranges of a and b. The Kramers rate r_k is the twice of signal frequency f_0 when resonance occurs [32].

$$r_k = \frac{a}{\sqrt{2}\pi r} e^{-\frac{a^2}{4bD}} = \frac{a}{\sqrt{2}\pi r} e^{-\frac{\Delta V}{D}} = 2f_0$$
(8)

where r is the damping factor of the second order duffing equation in (9) and r_k is the Kramers rate.

$$\frac{d^{2}x}{dt^{2}} - r\frac{dx}{dt} = -V'(x) + s(t) + n(t)$$
(9)

where x is the system output signal, s(t) is the input signal, and n(t) is the background noise.

The potential height ΔV affects the transition of the particle between the two potential wells and then the accuracy of signal frequency detection. Derived from (8), the relationship between the frequency f_0 and potential height ΔV is (10). Hence, ΔV needs to change while the input signal frequency changes. ΔV should decrease to help the particle to complete the transition between the two potential wells when the signal frequency f_0 increases. When the signal frequency f_0 decreases, ΔV should increase to reduce the speed of particle transition between the two potential wells, which can make the output signal frequency decrease and let

it equal to the weak input signal frequency.

$$f_0 = \frac{a}{2\sqrt{2}\pi r} e^{-\frac{\Delta V}{D}} \tag{10}$$

The relationship between the values of two adjacent signal frequencies is $\frac{f_b}{m} < f_c < m \times f_b$, where *m* is a real number greater than zero. f_b is the signal frequency before the frequency changes, and the current frequency is f_c . Hence,

$$\frac{f_b}{f_c} \in \left(\frac{1}{m}, m\right) \tag{11}$$

Set $\Delta V_n = \frac{\Delta V_c - \Delta V_b}{D}$, where ΔV_b is the optimal potential height before the frequency changes and ΔV_c is the optimal potential height for the current frequency. Hence,

$$\Delta V_n \in \left(\ln \left(\frac{a_c}{m \times a_b} \right), \ln \left(\frac{m \times a_c}{a_b} \right) \right)$$
(12)

where a_b is the optimal value of parameter a before the frequency changes and a_c is the optimal a for the current frequency. When f_0 increases,

$$\begin{cases} \Delta V_n \in \left(\ln \left(\frac{a_c}{m \times a_b} \right), 0 \right), & \frac{a_b}{m} \le a_c < m \times a_b \\ \Delta V_n \in \left(\ln \left(\frac{a_c}{m \times a_b} \right), \ln \left(\frac{m \times a_c}{a_b} \right) \right), & a_c < \frac{a_b}{m} \end{cases}$$
(13)
$$0, & a_c \ge m \times a_b$$

When f_0 decreases,

$$\begin{cases} \Delta V_n \in \left(0, \ln\left(\frac{a_c}{m \times a_b}\right)\right), \ \frac{a_b}{m} \le a_c < m \times a_b\\ \Delta V_n \in \left(\ln\left(\frac{a_c}{m \times a_b}\right), \ln\left(\frac{m \times a_c}{a_b}\right)\right), \ a_c \ge m \times a_b \\ 0, \ a_c < \frac{a_b}{m} \end{cases}$$
(14)

Generally, when $\frac{a_b}{m} \leq a_c < m \times a_b$

$$\begin{cases} \Delta V_n \in \left(\ln\left(\frac{a_c}{m \times a_b}\right), 0 \right), \text{ if } f_0 \text{ increases} \\ \Delta V_n \in \left(0, \ln\left(\frac{a_c}{m \times a_b}\right) \right), \text{ if } f_0 \text{ decreases} \end{cases}$$
(15)

Hence, when f_0 increases,

$$\Delta V_c \in \left(\Delta V_b + D \times \ln\left(\frac{a_c}{m \times a_b}\right), \Delta V_b\right)$$
(16)

when f_0 decreases,

$$\Delta V_c \in \left(\Delta V_b, \Delta V_b + D \times \ln\left(\frac{m \times a_c}{a_b}\right)\right) \tag{17}$$

Because $\Delta V_c = \frac{(a_c)^2}{4b_c}$, where b_c is the optimal system parameter b for the current frequency. Hence,

$$\begin{cases} b_{c.min} = \frac{(a_c)^2}{4\Delta V_{c.max}} \\ b_{c.max} = \frac{(a_c)^2}{4\Delta V_{c.min}} \end{cases}$$
(18)

where
$$\Delta V_{c.min} = \Delta V_b + D \times \ln\left(\frac{a_c}{m \times a_b}\right), \ \Delta V_{c.max} =$$

$$\Delta V_b + D \times \ln\left(\frac{m \times a_c}{a_b}\right)$$
. Therefore, $b_c \in (b_{c.min}, b_{c.max})$.

IV. SIMULATIONS

For the input signal, we set the amplitude A = 0.1 and frequency $f_0 = 0.01$ Hz. The signal sampling frequency f_s = 10 Hz, and the number of signal sample is l = 10000. The population size of genetic algorithm M = 100, crossover probability $p_s = 0.6$, and mutation probability $p_m = 0.001$. The searching ranges of system parameters a and b are $[0.0001 \sim 20]$ and $[0.0001 \sim 1000]$, respectively.

First, the background noise is assumed to follow zero mean Gaussian distribution with standard deviation $\sqrt{2D}$, and let D = 1 to verify that the SR system can improve the SNR_o . The time domain and frequency domain diagrams of the received signal and output signal are shown in Fig. 4. From Fig. 4. (a), when the noise intensity D = 1, it is observed that, due to the noise, the received signal appears non-periodic although the pure original signal is periodic. The periodicity of received signal r(t) from the time domain waveform is not obvious, and the original cosine signal s(t) is completely submerged in the background noise. The spectrum amplitude of target frequency $f_0 = 0.01$ Hz is not the biggest and smaller than that of some other frequencies in Fig. 4. (c). Therefore, the target frequency f_0 could not be detected from the received signal r(t) . However the time domain waveform of the output signal has obvious periodicity in Fig. 4. (b), and the spectrum amplitude of target frequency f_0 is significantly higher than that of other frequencies in Fig. 4. (d). The $SNR_i = -27.6647$ dB and the SNR_o = -8.6511 dB. The SNR_o increases by 19.0136 dB. Therefore, the SNR_o of weak signal with strong background noise can be increased and the target frequency can be detected by SR system.

A. The performance of SR System with the CSNR Index

We compare the performance of SR systems with the CSNR, PMV, and WPSK indexes for weak signal frequency detection. With 500 trials, the different frequency detection



Fig. 4. (a) Received Signal in Time Domain, (b) Output Signal in Time Domain, (c) Received Signal in Frequency Domain, (d) Output Signal in Frequency Domain.

probability p of SR systems with different indexes are shown in Fig. 5, denoted by p_c , p_p and p_w , respectively. The detection probability p decreases with SNR_i decreases. p_c is higher than p_p and p_w when the SNR_i ranges from -32 to -19 dB. This indicates that the CSNR index is more robust. p_c and p_w are approximate to 1 and higher than p_p when the SNR_i ranges from -19 to -16 dB. From Fig. 5, the SNR_o of SR system with the CSNR index is improved by around 2.3 dB and 6.1 dB compared to the output by PMV and WPSK indexes, respectively when detection probability p is around 0.9.

We compare the sensitivity of SR systems with the CSNR, PMV, and WPSK indexes, respectively, regarding the signal frequency change. Let noise intensity D = 1 and the input signal frequency f_0 varies from 0.01 to 0.3 Hz with step of 0.01 Hz. The detection results are shown in Fig. 6 and the detection probability p of SR systems with the three indexes decreases with the input signal frequency increases, which verifies that the SR system is adaptive to the detection of low frequency signal. p_c is higher than 0.8 and p_p is between 0.5 and 0.8. In addition, p_w is lower than 0.5 and decreases rapidly. Therefore, the SR system with CSNR index is less sensitive to the change of signal frequency and more robust than the SR systems with PMV and WPSK indexes.

B. Time Efficiency of Single Frequency Signal Detection

Let $\tan \theta = \Delta V/x_m = 1/30$ in Fig. 1. We compare the signal detection probability p and time T by SR systems with the different searching ranges of parameter b and different input signal-to-noise ratios. The detection results are shown in Fig. 7. It indicates that the detection probability p of weak signal frequency with different searching ranges of system parameter b decreases with the SNR_i . The detection probability p with different searching ranges of system parameter b are no obvious difference basically when SNR_i rangs from -32 to -16 dB. From Fig. 7. (b), it is clear that the detection time T with different searching ranges of system parameter b increases when SNR_i varies from -32 to -21 dB and then decreases when SNR_i varies from -21 to -16 dB. It indicates that when the signal amplitude A = 0.1, frequency $f_0 = 0.01$ Hz, and the



Fig. 5. The Single Frequency Signal Detection Probability by SR Systems with Different Indexes and Different Input Signal-to-Noise Ratios, where the Red, Green and Blue Curves are the Detection Probability with the CSNR, PMV and WPSK Indexes, respectively.



Fig. 6. The Single Frequency Signal Detection Probability by SR Systems with Different Indexes and Different Signal Frequencies, where the Red, Green and Blue Curves are Detection Probability with the CSNR, PMV, and WPSK Indexes, respectively.

 $SNR_i = -21$ dB, the SNR_o of SR system will be maximized. The trends of three detection time curves are similar to the SNR_o with respect to the noise intensity D (see Fig. 2).



Fig. 7. With the Different Searching Ranges of Parameter *b*, the Single Frequency Signal Detection Probability and Detection Time with CSNR Index and Different Input Signal-to-Noise Ratios.

Denote the optimal noise intensity by D_o . When $D < D_o$, the SNR_o of SR system increases with noise intensity D. In this situation, when noise intensity D increases, the SR system needs more time to detect the weak signal. When $D = D_o$, the SR system has the maximal SNR_o and the detection time of signal frequency should be maximized. When $D>D_o$, the SNR_o of SR system decreases with the noise intensity D. The output signal of SR system is suboptimal and the detection time will decrease when noise intensity D increases. From Fig. 7. (b), the detection time with the upper and lower searching ranges of parameter b is less than that of the other searching ranges of parameter b obviously. Therefore, by bounding the searching range of parameter b, the detection time T can decrease. When the signal frequency changes with D = 1 and f_0 varies from 0.01 to 0.3 Hz with step of 0.01 Hz, the signal detection probability p and time T of SR systems with different searching ranges of parameter b are shown in Fig. 8. It is observed that the signal frequency detection time is decreased when the method of bounding the parameter b searching range is applied.



Fig. 8. With the Different Searching Ranges of Parameter *b*, the Single Frequency Signal Detection Probability and Detection Time with CSNR Index and Different Signal Frequencies.

C. Time Efficiency of Frequency-Hopping Signal Detection

For the input frequency-hopping signal, set amplitude A = 0.1, and the signal hopping frequency is [0.01, 0.06, 0.01, 0.02, 0.04, 0.08, 0.05, 0.10, 0.15, 0.13] Hz, respectively. The signal sampling frequency $f_s = 10$ Hz, and the number of sampling points of signal for each frequency is l = 10000. The change of signal frequency is shown in Fig. 9. (a). SNR_i ranges from -24 to -16 dB. With 100 trials, the signal detection time T with different searching ranges of parameters a and b is shown in Fig. 9. (b), and the detection probability p for each frequency is 1. It can be concluded that the detection time for frequency-hopping signal can decrease by SR system when the method of bounding the parameters a and b searching ranges is applied.



Fig. 9. (a) The Frequency of Original Frequency-Hopping Signal. (b) With the different Searching Ranges of Parameters a and b, the Frequency-Hopping Signal Detection Time by SR System with the CSNR Index.

V. EXPERIMENTS

A. Single Frequency Signal Detection

The experimental site is located at the seaside of Xinghai Park in Dalian City. The signal of a motor with a fixed frequency is used as the weak signal to be detected. A mobile phone is used as the receiving device. The signal sampling frequency $f_s = 8000$ Hz. The motor and phone are placed below the sea surface around 0.5 m and the distance between them is around 2 m. The received signal r_s is shown in Fig. 10. r_s is amplified by a factor g, g = 3. We select three periods of signals r_i (i = 1, 2, 3) from r_s . The number of signal samples for each period is l = 10000. The sample points are $[325000 \sim 335000], [356000 \sim 366000], [450000 \sim 460000]$ for r_1 , r_2 and r_3 , respectively. The detection results are shown in Tab. I and Fig. 11. The detected frequency $f_0' = 0.028$ Hz by SR system and the actual signal frequency can be obtained by $f_0 = f'_0 \times R = 56$ Hz, where R is the ratio of down-converting the high frequency of actual signal into a low frequency, R=2000. From Fig. 11, the frequency of weak signal r_1 can be detected by SR systems with CSNR, PMV, and WPSK indexes, respectively. For the output signal, the spectrum amplitude of frequency f'_0 with the CSNR index is higher than that by each of the other two indexes. From Tab. I, the SNR_o by SR system with the CSNR index is higher than the output by the other two indexes, and the detection time of single frequency by SR system with the upper and lower searching ranges of parameter b is less than that when no

searching range is set for parameter b or only lower searching range is set.



Fig. 10. Original Received Signal r_s

B. Frequency-Hopping Signal Detection

The signal of a motor with dynamic frequency change is used as the weak signal to be detected. The signal sampling frequency $f_s = 44100$ Hz. The frequency of the motor is adjusted dynamically by a knob. The motor and phone are place below the sea surface around 0.5 m and the distance between them is around 4 m. The received signal r_s is shown in Fig. 12. r_s is amplified by a factor g, g = 200. We select ten periods of signals r_i (i = 1...10) from signal r_s . The number of signal samples for each period is l = 10000. Then the ten periods of signals are combined into a new frequency-hopping signal s. From Fig. 13. (a) and Fig. 14. (a), the periodicity of signal s is not obvious. However, the output signals by SR systems with different parameters searching ranges show a strong periodicity (see Fig. 13. (b), (c), (d)). The time-frequency spectrum of the output signals by the SR systems with different searching ranges of system parameters a and b are shown in Fig. 14. (b), (c), (d), where the color brightness for each frequency in the signal spectrum indicates the magnitude of the normalized spectrum amplitude. In each of four cases, the target frequency is detected, i.e., the spectrum amplitude of the target frequency is the maximum and it is indicted by the brightest color. The frequency-hopping signal s is detected in four cases: 1) frequency-hopping signal s; 2) no searching ranges set for a and b; 3) set searching range of parameter b for single frequency signal; and, 4) set searching ranges of a and b for frequency-hopping signal. The detection results are the same for the four cases, however the periodicity of system output signal for the case 2), 3) and 4) are more strong than case 1). The detection frequencies are f' = [0.063945, 0.134505,0.055125, 0.063945, 0.072765, 0.059535, 0.14112, 0.06615, 0.090405, 0.04851] Hz by SR systems with different searching ranges of parameters a and b, respectively. The actual signal frequencies can be obtained by $f = f' \times R = [127.89, 269.01,$ 110.25, 127.89, 145.53, 119.07, 282.24, 132.30, 180.81, 97.02] Hz, where R=2000. The detection time of the frequencyhopping signal s with different searching ranges of parameters are 307.374s, 282.517s, and 226.736s, respectively. It indicates for frequency-hopping signal that the detection time by SR system by setting the searching ranges for a and b decreases by 80.638s and 55.781s, respectively, than that produced when no searching range is set or only the searching range for parameter b is set.

	r_1		r_2		r_3	
Different						
indexes	SNR_o/dB	T/s	SNR_o/dB	T/s	SNR_o/dB	T/s
$\overline{\text{CSNR}_{no}}$	-9.3987	16.7440	-8.2307	9.1730	-9.6321	9.5680
$CSNR_l$	-9.7140	10.6470	-8.5466	13.6340	-9.8430	18.5040
CSNR _{ul}	-9.3512	8.2720	-8.1565	8.5050	-9.6743	8.4370
PMV	-9.7326	15.1588	-8.6778	10.3360	-9.7843	8.7956
WPSK	-9.8321	13.7259	-8.8342	9.0453	10.3420	9.5723

 a CSNR_{no} is the condition with the CSNR index and the no searching range set.

^{*b*}CSNR_{*l*} is the condition with the CSNR index and the only lower searching range set for *b*.

^cCSNR_{ul} is condition with the CSNR index and the upper and lower searching ranges set for b.



Fig. 11. The Detection Results of Single Frequency Signal r1 by SR Systems with Different Indexes and Searching Ranges of Parameter b.



Fig. 12. Original Received Signal r_s .

VI. RESULTS AND DISCUSSION

The performance of weak signal detection by SR system with the CSNR index is verified by simulations and experiments. The frequency detection probability of SR systems with CSNR, PMV, and WPSK indexes are denoted by p_c , p_p and p_w , respectively. In simulations, p_c of weak signal with the CSNR index is 1 when the SNR_i is higher than -26 dB, and p_c is as high as 0.9 when $SNR_i = -27.5$ dB. p_c is higher than p_p and p_w when SNR_i varies from -32 to -19 dB. p_c and p_p are approximate to 1 and higher than p_w when SNR_i is $[-19 \sim -16]$ dB. When SNR_i = -26 dB, the performance of SR system with the CSNR index is insensitive to the change of input signal frequency. p_c is higher than 0.8 and p_p is between 0.5 and 0.8 when the input signal frequency f_0 varies from 0.01 to 0.3 Hz with step of 0.01 Hz. However, p_w is lower than 0.5 and p_w decreases rapidly. With the searching range set for system parameter b, the detection time of single frequency signal with the CSNR index decreases. The SNR_o of SR system with CSNR index is higher than the output by PMV and WPSK indexes in the same condition. For frequency-hopping signal, with the searching ranges set for system parameters a and b, when SNR_i varies from -24 to -16 dB, the signal detection time will decrease significantly. The experimental results are consistent with the simulation results.



Fig. 13. The Signal in Time Domain. (a) Frequency-Hopping Signal s, (b) the Output Signal with no Searching Range Set, (c) the Output Signal with Searching Range Set for Parameter b only, (d) the Output Signal with Searching Ranges Set for Parameters a and b.



Fig. 14. The Signal in Time-Frequency Spectrum. The X-Label Represents Signal r_i (i = 1...10) and Y-Label Represents the Output Signal Frequency (from 0 to 500 Hz). (a) Frequency-Hopping Signal s, (b) the Output Signal with no Searching Range Set, (c) the Output Signal with Searching Range Set for Parameter b only, (d) the Output Signal with Searching Ranges set for Parameters a and b.

VII. FUTURE PLANS AND IMPROVEMENTS

The future plans are summarized as follows. First, the machine learning method can be combined with the genetic algorithm in this paper to further improve the detection time efficiency of unknown signals. Second, we can use underwater sonar array to improve the signal detection probability. The experimental verification part needs to be improved. I hope to conduct experiments in deep sea in the future to obtain more diverse and accurate underwater signals.

VIII. CONCLUSION

In this paper, a new index, called CSNR, is proposed to detect the frequency of unknown underwater signals based

on SR theory with genetic algorithm, and the method of bounding searching ranges of system parameters a and b is presented to reduce the detection time. The performance of weak signal detection by SR system with the CSNR index is verified by simulations and experiments. The frequency detection probability of SR systems with CSNR, PMV, and WPSK indexes are denoted by p_c , p_p and p_w , respectively. The results show that p_c is higher than p_p and p_w . In addition, the performance of SR system with the CSNR index is insensitive to the change of input signal frequency. With the searching ranges set for system parameters a and b, the signal detection time will decrease significantly in simulations and experiments. In conclusion, the SR system with the proposed CSNR index and parameter searching ranges outperforms SR systems with PMV and WPSK indexes in terms of detection probability and detection time. Therefore, the contributions proposed in this paper are of positive significance to the detection of underwater weak signals in practical applications.

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