# Ọdigbo Metaheuristic Optimization Algorithm for Computation of Real-Parameters and Engineering Design Optimization 

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#### Abstract

This paper proposes a new population-based global optimization algorithm, Odigbo Metaheuristic Optimization Algorithm-OMOA, for solving complex boundedconstraint/single objective real-parameter problems found in most engineering and scientific applications. It's inspired by the human socio-cultural informal discipleship learning pattern inherent in the behavior of the Ndigbo peoples; the subject primary (Nwa-ahia), in mercantile cycle grows to a secondary (Mazi) owing to the intuitive stratagem (dialect - Igba) embedded in an aged-long cultural model "Igba-ọsọ-ahịa" (meaning, strategic marketing skills, and practice). The model mimics the search routine for satisfying a customer's need in the market, built into exploration and exploitation applied in the mathematical model. About 30 complex classical unconstrained functions are tested, comparing results with that of five similar state-of-the-art algorithms. Also, 29 CEC-2017 single objective real constraint benchmark serious dimensional problems were simulated and compared against the winners of that competition. Validation includes statistical (t-test, p-value) comparison and for 50 Dimension constraint problems as OMOA demonstrated superior performance. TCS $(\mathbf{9 . 1 8 \%})$, WBP ( $6.3 \%$ ), PVDP (601\%), RGP (319\%), RBP ( $\mathbf{7 6 0 \%}$ ), GTCD (202\%), HIMMELBLAU ( $\mathbf{4 \%}$ ), and CDP ( $\mathbf{8 8 . 1 2 \%}$ ) are the improvements made on 8 CEC-2020 engineering real design problems against the former best performances; OMOA is simple to implement, replicate and applicable across domains. Also, some new, improved optimum was obtained in Shubert and Schaffer 4 function compared to the global optimums.


Keywords-Human socio-cultural; nature-inspired; informallearning; global optimization

## I. InTRODUCTION

Humans and animals face challenges within their time and space of habitation, and they attempt to solve the challenges by making decisions and selecting and combining variables influencing the conditions. The challenges range from simple to difficult-complex ones, but the satisfaction derived from attaining the goal motivates effort for solution pursuant [1]. Engineering has availed very good solutions for small scaled problems using exact methods, but such fails when the problem becomes special and high dimension, become very costly and time consuming [2]. Meanwhile, the study of nature showed complex problems solved by meta-ideas and heuristics. The aesthetics that describes the meta-heuristics provide solutions that are near-optimal yet scalable with problem dimensions [3] despite the difficult procedural
uncertainties [4]; the huge difficulty is associated with the mapping of routines called intelligence from rules or heuristics that describe events of nature which falls in a multidisciplinary field [5, 6]. Research in this direction has yielded several methodologies for solving engineering problems, yet more are anticipated [6]. This work aims to address some multidisciplinary domain concerns; a significant gap in balancing exploitation and exploration in populations of solution search impacts the state-of-art. Also, most recent works have scantily described the critical analogies of the metaphors that reflect the aesthetics of the target nature's source with the derived mathematical models, while the majority favors hybridization. Also, only a handful of the existing algorithms had human behavior metaphors, which this work proposes. Based on life science, a simple category of existing solutions could be into biological and non-biological (abiotic) hybrids, Bio-Abiotic hybrids, Bio-Bio hybrids, and Abiotic - Abiotic hybrids; however other literature may use alternative categorizations such as Swarm, Evolutionary, and Human intelligence. Genetic algorithms (GA) led the natural biological methods [7]. Particle Swarm Optimization (PSO) is inspired by flocks of birds and schools of fish [8] [9]. A few others due to space constraints are; Artificial Bee Colony from bee foraging [10]; Ant Colony [11]. In literature, numerous applications of the metaheuristics includes scheduling, loading, packaging, design, and control [12], image processing, amongst numerous others. The abiotic category is based on artificial physical experiences, such as Tabu Search, which made use of the creation of a tabu list [13]; Water Evaporation Optimization (WEO), mimicking the evaporation of water [14, 15]; JAYA mimicking the gravitation towards success [15]; Atomic Orbital Search (AOS) [16], etc. Some modified/hybrids are; Grey Wolf and PSO [17] gave (GWOPSO), MOGSABAT [18] from the multiobjective gravitational search algorithm, and the echolocation ability of the bat algorithm [19]. Many other metaheuristic methods can be found $[20,21]$. OMOA is a new strategy proposed by this work; the data is from the human population shown in Section II. The aesthetics are based on informal learning. The mathematical relations are developed in Section III and experiments, results and discussions are also presented in Section III, while Section IV is the conclusion.

The data of this work is gathered from the Ndigbo people's mercantilism. This ideology is found in major Market setups across the World, where Ndigbo are found in huge populations

[^0][22, 23]. They cooperate and maintain this characteristic ideology they call "igba"; meaning stratagem. [24, 25]. The aesthetics; every male is disciple/given-chance-to-handson/learn informally in commerce backed by some form of agreement [26]; a model known to them as "Igba-ọọ-ahịa" which means strategic marketing skills acquisition and practice. Ahịa (market) is a solution space and holds all history of exploitations and explorations through Igba-ọsọahịa model [27]. There exist huge risks and sacrifices, but the Ndigbo tolerates them [27].

## A. OMOA Algorithm Description

In the Ahịa environment, the ultimate is to become a Mazi; The initial population is generated randomly as Ahịa-size. This is the "initialization mode"; The readiness, practicing, discipline, trading, cooperation, and the reluctance of the agents (known as ụmụ-ahịa in Igbo) is adjusted against the new environment each day; [from start-transduction mode to update-matching mode].

## II. Modeling Data and Aesthetics

The work started with a collection of data from a local ahịa; the data is found at https://data.mendeley.com/datasets/ $\mathrm{wt} 3 \mathrm{vt} 72 \mathrm{mph} / 1$. A few assumptions and facts extracted from data include but are not limited to the following parameters:

1) NORMS: (i) Every Mazi Own at least one shop. (ii) Every Nwa-ahịa is attached to a Mazi, a shop, and an ahịa. With an agreement, (iii) Death or risk are inevitable etc.
2) AXUMES: (i) Every Nwa-ahịa must satisfy a certain set percent of discipleship requirements to become a Mazi.
3) FACTS and Probable: (i) Certain Nwa-ahịa may succeed, fail, die, or get impeded. (ii) Certain Mazi may become greedy and unjust. (iii) Certain Ụmụ-ahịa had gotten second and third chances to make up, and many ahịa exist.

## B. Sample Size of Selected Market

Data in Table I shows a snapshot of the collection, and the values represent the sub-total in each case. For example, the column representing "Japan"; "JAPANLINE"; "shops:35"; Parts: [12: "Nissan", 23: "Toyota Accessories", NULL:" x"].

## C. The Model - Ahịa

The visualization of the setup of ahịa as a system (inputs, process, and outputs) schematically looks like Fig. 1 (left, right)

Fig. 1(a) shows Ahịa [ $n+9]$ described in Fig. 1(b) explicitly; the lines show the nonlinear relationships. The inner layers are shops and are associated with entities enlisted. The local Ahịa are networked across major cities in Nigeria (Ibadan, Lagos, Onitsha, etc.) which affiliates to extensions in Countries like Japan and Germany. The Ahịa primary agent (humans) are ụmụ-ahịa, and secondary are ndi-ọsọ-ahịa, Mazi, Bankers, customers (Regular and Non-Regular), suppliers, forwarding and clearing and etc. Meanwhile, the number of decision variables in sales, storage, borrowing etc., varies with constraints of environments like the cash flow, religion, and local/global politics etc.; taking shop 9 - GermanyLine Fig. 2; it comprises 1 -Mazi, 5 - Ụmụ-ahịa, 1 - Onye-ọsọ-ahịa, 12 -

Regular Customers, 100 - Emergency Customers and trading on Benz-Spare Parts as shown.

TABLE I. SAmpled Data From a Market and Shop Distributions

| Object | $\begin{gathered} \hline \text { JAPA } \\ \mathbf{N} \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { TOYO } \\ \text { TA } \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { GERMA } \\ \text { NY } \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathbf{A B} \\ \mathbf{A} \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { BAMEN } \\ \text { DA } \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Mazi | 35 | 43 | 101 | 122 | 199 |
| UTmu-ahịa | 210 | 250 | 591 | 696 | 1162 |
| Ndi-ọso-ahịa | 35 | 43 | 101 | 122 | 199 |
| Regular Customers | 2204 | 2786 | 5039 | $\begin{aligned} & 1926 \\ & 4 \\ & \hline \end{aligned}$ | 23616 |
| Emergency Customers | 2859 | 4646 | 10100 | $\begin{aligned} & 1559 \\ & 5 \end{aligned}$ | 20168 |
| Shops |  |  |  |  |  |
| Nissan and Toyota Parts | 12 | x | x | x | x |
| Toyota Accessories | 23 | x | x | x | x |
| Toyota-Spare-Parts | x | 43 | x | x | x |
| Benz-Spare-Parts | x | x | 22 | x | x |
| Audi Parts | x | x | 31 | x | x |
| Gold and Volkswagen | x | x | 24 | x | x |
| Benz Engine | x | x | 11 | x | x |
| Benz-Dashboard and Accessories | x | x | 13 | x | x |
| Cloth and Okrika | x | x | x | 122 | x |
| Tokunbo <br> Phones Fridges  | x | x | x | x | 199 |



Fig. 1. Ahịa business model and networks.


Fig. 2. Snap off idumọta sampling.
In obtaining the adjacency list from the data, assumptions made included (1) (1/0 means connected/not-connected)
respectively; (2) also shop data is deterministic data at capture time, the network of the single shop nine(9) is modeled, and the simulation - Bayes graph is as shown


Fig. 3. The schematic representation of the network traffic.
The complex network of the shop ( 54500 edges, 364 nodes), on a market day named Orie; Fig. 3 is made. It depicts the intense cognitive field (energy) of nonlinear relationship maps responsible for transduced processes with experience (edges) of ụmụ-ahịa (nodes) that Orie day. Daily customer satisfaction time monotonically decreases with increasing edges, even with constraints in cycles. Beyond shop 9, thousands of shops contribute to the ahịa data; the computer structural model is shown in Fig. 4.


Fig. 4. Ahịa environment across many shops.
S1, S2, m1, m2, m3, m4, and M2 represents: shops 1, ndi-ọsọ-ahịa, nwa-ahịa-1, nwa-ahịa-2, nwa-ahịa-3, nwa-ahịa-4, and many other distance ahịa (markets). The updates are processes of the ụmulahịa transforming on every market day (Ọrie, Afọr, Nkwọ, Eke). The colours is evidence uncertainty.

## D. Initialization of Population (Market-Size)

OMOA; with the decision variables, Igba-ọsọ-ahịa and Ddimensions, the solution vector in the ahịa can be represented as (1).

$$
\begin{equation*}
\text { Mazi }=\left[x_{1}, x_{2}, x_{3}, \ldots, x_{D}\right] \tag{1}
\end{equation*}
$$

The fitness value of each Mazi will be computed as a vector of (2);

$$
\begin{equation*}
f(\text { Mazi })=f\left(x_{1}, x_{2}, x_{3}, \ldots, x_{D}\right) \tag{1}
\end{equation*}
$$

For instance, a new shop with new ụmụ-ahia (ages of 3 and 8 yrs .), some constraints of this age group include (a) Nostalgic energy in early months, inherent childishness (comprises of untargetted and undirected energies): chaotic sleeping patterns, food pattern, and desires for the first few months persist. But discipleship (hands-on, disciplinary
actions, corrections, task handling, rewards) between 1 and 5 years changes their energies to focused excitement; next is integrity and trust test; Each nwa-ahịa has a position and cost affected by such constraints and uncertainty in capacity, inductiveness, and reluctance. The population is generated using (3).

$$
\begin{equation*}
p o p=\Phi(M, D) \tag{3}
\end{equation*}
$$

The $\Phi$ is a random generator, M is the market population (pop), and D is the dimension. The pseudocode is shown below.

## Initial parameters

$$
\begin{aligned}
& \text { Initialize the structure for the empty individuals } \\
& \text { Initialize population array } \\
& \text { while (not termination) Do } \\
& \quad \text { generate uniform random population with } \\
& \text { bounded size of market } \\
& \text { evaluate the cost of the individual } \\
& \text { update individual population } \\
& \text { end while } \\
& \text { return best solution }
\end{aligned}
$$

## E. Mathematics of Igba-ọso-ahịa

Fig. 5(a) in 3-dimensional space during the search is shown in 2-Dimension as Fig. 5 (b) as agents move to satisfy customers' scarce demand for "gold" and "leather" as in Fig. 4 to exploit $S_{1}$ and explore $S_{2}$.


Fig. 5. Iggba-ọsọ-ahịa cooperation by to find gold.
They cooperate, meet set thresholds, and satisfy the customer to get his Gold. Initializing a new Mazi, a new shop, and his contribution to the solution space will be given by (4).

$$
\begin{equation*}
U_{n}=f\left(X_{1}\right) \tag{2}
\end{equation*}
$$

Combining equation (1) and (2);

$$
U_{n} \leftarrow\left\{\begin{array}{c}
x_{i} \in\left\{x_{r}\right\} \text { mazi with new umu-ahia }  \tag{3}\\
x_{i} \in X_{1} \quad 1 \text { mazi, without umu-ahia }
\end{array}\right.
$$

Some of the major constraints (3) as mentioned in Section II. n; the number of generations - the stopping criteria, $r$ indicates $x$ is random. Mazi cost alone in trade without ụmụahịa in the cycle of Ahịa days (6) resolves to a fitness vector:

$$
\begin{equation*}
U_{n}=X_{n-1} *(P(i,:)) \tag{6}
\end{equation*}
$$

Where $P(i,:)$ is the cost of Mazi in the population of $\mathrm{P}, i$ cycles of Ahịa days, and the transmute of Mazi's energies via the training processes. At the same time, the umụ-ahịa adopt the emitted energies originating from multidiscipline like phycology, social tactics, resilience, experience, transactional techniques, relationship with customers, banks, etc., The differences compared to theirs cut across domains and, by analogy, involve transduction [28]. This process is given by a resemblance of balancing potentials and kinetics.

$$
\begin{equation*}
T=\operatorname{rand}(1, D) *(P(p,:))-1 / 2 * E f *\left(X_{r}\right) \tag{4}
\end{equation*}
$$

Where $P(p,:)$ in (4) is the cost of the new population at time $\mathrm{p}, E f$ is the energy factor, while the $X_{r}$ random ụmụahịa cognitive state of five analogous Bayesian energies interacting actively in a shop.

$$
\begin{array}{r}
X_{r}=X_{r+i}+1 / 8 * E f *\left(X_{r+i-1}\right) \\
X_{r+i-1}=X_{r+\Delta(i-1)}+1 / 40 * E f * X_{r+\Delta(i-1)} \\
X_{r+\Delta(i-1)}=1 / 80 * X_{r+\Delta(i-n)} \tag{7}
\end{array}
$$

Equations (5), (6) and (7) are all nonlinear cognitive vectors, and ratios of series $[1 / 8,1 / 40$, and $1 / 80]$ of time divisions (could take any ratio as they are probabilities of random events, recall a state ranges from 0 to 1 ), $i, r$ remain the same; visually, a huge network ensues as shown below.


Fig. 6. Cognitive correlations between nwa-ahịa (PN) to any.
Fig. 6 clusters N1 ụmụ-ahịa with each other, and N2 and N3 are the clusters with customers. The probabilistic behavior of the interaction (edges) shows the very interesting transition of the ụmụ-ahịa (nodes) progress in the network in Fig. 7.


Fig. 7. Progress of cognitive signature on ụmụ-ahịa character.
Current time $t$; the previous timestamps as the selected node (60). Search in a generation gives (11).

$$
\begin{align*}
X_{r}= & X_{r+i}+1 / 8 * E f *\left(X_{r+\Delta(i-1)}+\ldots\right. \\
& \left.\left.1 / 40 * E f\left(1 / 80 * X_{r+\Delta(i-n)}\right)\right)\right) \tag{8}
\end{align*}
$$

Where updates at $r+i$ taken during iteration. The compact dynamics (12); mimics a rhythmic nodding to music and stratagem - ịgba, which gives.

$$
\begin{equation*}
U_{n}=U_{n-1}+T_{n-1} * X_{r} \tag{12}
\end{equation*}
$$

Where ${ }^{U} n$ is a vector of emergent solutions. The threshold facilitates ụmụ-ahịa exploration; disciple-Rhythm $r D$ known as discipleship compliance, given by (13).

$$
U(i j)=\left\{\begin{array}{l}
u_{m}^{j} \text { if } m \leq r D \text { OR } j=\delta  \tag{9}\\
x_{m}^{j} \text { if } m>r D \text { AND } j \neq \delta
\end{array}\right.
$$

Where m is a random number [ 0,1 ], delta $\delta$ has the same dimension and size as the solution but is pseudorandom. This cooperation serves as the bond linking one source to another [23, 29]. Mazi; sometimes sacrifices profit for an improved customer base and to escape the local optima trap by analogy as Igba-ọsọ-ahịa updates; objectives of the fitness bound the strategy as given in Fig. 8.


Fig. 8. Boundary strategy.
Constraints are bounded as in $\mathrm{A}, \mathrm{N}$ collapse to upperbound (UB) in B, and N collapse to lower-bound (LB) as shown in Fig. 8. Finally, methodic update results to best solutions shown.

$$
\left.\begin{array}{r}
x_{i}=U_{i}  \tag{10}\\
f_{i}=f_{U_{i}}
\end{array}\right\} \text { if } f_{U_{i}}<f_{i}
$$

$$
X \text { and } f \text { remainsthe sameif } f_{U_{i}}>f_{i}
$$

Where (10); $f_{U i}$ is the fitness function from the best cost of the discipleship and adjustments made (error correction), while $f_{i}$ is the best solution fitness of the original objective function, which is optimal.

## F. Graphical Flow of OMOA

The ụmulahia can be considered as moving particles [3032]. Mazi realization comes after generations of successful cycles [33]; rather than unhealthy competition, all ụmụ-ahịa depends on each other; The main body's pseudocode (2) during iteration is as follows:


Fig. 9. Odịgbo metaheuristic optimization algorithm - OMOA and pseudocode.

The flow chart of Fig. 9 shows the methodology for applying the OMOA algorithm. The subsequent sections discuss applications.

## III. Application of OMOA on Benchmark Functions

Most metaheuristic algorithms use Pattern Matrix, and the solutions are identified as those that improved through the number of generations up until the convergence time of the simulation. OMOA inherent energy synergy principles.

1) Default parameters are used
2) 30 independent runs were used for Unconstraint Benchmark, 50 for constraint functions. The parameters for the engineering designs are as stated in the referenced literature provided
3) The total number of cost function evaluations is $1000 \cdot \mathrm{n} \cdot \mathrm{M}$, where $\mathrm{M}=10$ is the number of iterations. The logarithmic Scale was considered for visualization due to its convenience and compact.
4) For the Constraint problems as depicted by the competition, a solution value less than $10^{-8}$ is treated as zero; several performance indicators for solution values are used: best, worst, mean, and standard deviation (Std). Test for convergence time also provided;

## A. Experiments and Comparison of Results

OMOA is compared with five of the best similar algorithms as shown in Table II. Their codes are in the open domain/available online. The choice of only five is being mindful also of the limited space constraints to publish results.

TABLE II. ALGORITHMS USED FOR VALIDATION

| S/N | Algorithm | Ref | Category |
| :--- | :--- | :--- | :--- |
| 1 | Harris Hawks Optimization <br> (HHO)-- 2019 | $[34]$ | Novel Idea |
| 2 | Moth Search (MS)-- -2018 | $[35]$ | Novel Idea |
| 3 | Elephant Herd Optimization <br> (EHO)-- 2015 | $[36]$ | Novel Idea |
| 4 | LSHADE-SPACMA ( A2) - <br> 2017 | $[37]$ | Hybrid/Modified |
| 5 | EBOwithCMAR (A3) ---2017 | $[38]$ | Hybrid/Modified |

The list in Table II is a competitive group; notably, $4-5$ won the CEC 2017 competition [39, 40].

## B. Experiment 1: Difficult Unconstraint Benchmark Functions

OMOA is validated on the existing established algorithms listed in Table II with about 30 difficult functions chosen with modality (unimodal to check and confirm exploitation strength, multimodal for diversity or exploratory capability of OMOA), Separability (possible separable and non-separable) and then multi-dimensionality (confirming search and exploratory strength of OMOA). The performance averages are visualized using boxplots. Further, the significance and statistical students test (t-test) was conducted for all algorithms, with a time complexity test. A subset of test benchmark functions with varying degrees of difficulty is used to substantiate that OMOA can exploit and explore the solution space and find the solutions for optimum. In Table III, unconstraint benchmark test functions are categorized in modality, Separability, and Dimensionality ( $\boldsymbol{N}$ ), also: $\boldsymbol{M}$ is the modality, $\boldsymbol{O}$ - Uni-modal; $\boldsymbol{I}$ - Multimodal, $\boldsymbol{S}$ is the Separability, $\boldsymbol{0}$ - Non-Separable; $\mathbf{1}$ - Separable.

TABLE III. Functions, Global Optimal Values, Bounds, and DIMENSIONS

| Fun(fn) | Fun-name | $\boldsymbol{S D}$ | $\boldsymbol{F}\left(\boldsymbol{x}^{*}\right)$ | $\boldsymbol{N}$ | $\boldsymbol{M}$ | $\boldsymbol{S}$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| F1 | Step | $[-5.12,5.12]^{n}$ | 0 | 30 | 0 | 1 |
| F2 | Sphere | $[-1,1]^{n}$ | 0 | 30 | 0 | 1 |
| F3 | Sum Square | $[-5.12,5.12]^{n}$ | 0 | 30 | 0 | 1 |
| F4 | Quartic | $[-6.0,6.0]^{n}$ | 0 | 30 | 0 | 1 |
| F5 | Beale | $[-5.0,5.0]^{n}$ | 0 | 2 | 1 | 0 |
| F6 | Easom | $[-100.0,100.0]^{n}$ | -1 | 2 | 1 | 0 |
| F7 | Matyas | $[-10.0,10.0]^{n}$ | 0 | 2 | 1 | 0 |
| F8 | Colville | $[-10.0,10.0]^{n}$ | 0 | 4 | 1 | 0 |
| F9 | Zakharov | $[-5.0,5.0]^{n}$ | 0 | 30 | 1 | 0 |
| F10 | Schwefel 2.2 | $[-10.0,10.0]^{n}$ | 0 | 30 | 1 | 0 |
| F11 | Schwefel 1.2 | $[-10.0,10.0]^{n}$ | 0 | 30 | 1 | 0 |
| F12 | Dixon Price | $[-10.0,10.0]^{n}$ | 0 | 30 | 1 | 0 |
| F13 | Bohachevsky 1 | $[-100.0,100.0]^{n}$ | 0 | 2 | 1 | 1 |
| F14 | Booth | $[-10,10]^{n}$ | 0 | 2 | 1 | 1 |
| F15 | Holder Table | $[-1010]^{n}$ | -19.2085 | 2 | 1 | 1 |
| F16 | Michalewicz 2 | $[0.0, \pi]^{n}$ | -1.8013 | 2 | 1 | 1 |
| F17 | Michalewicz 5 | $[0.0, \pi]^{n}$ | -4.6877 | 5 | 1 | 1 |
| F18 | Michalewicz 10 | $[0.0, \pi]^{n}$ | -9.6602 | 10 | 1 | 1 |
| F19 | Rastrigin | $[-5.12,5.12]^{n}$ | 0 | 5 | 1 | 1 |
| F20 | Schaffer2 | $[-100,100]^{n}$ | 0 | 2 | 1 | 0 |
| F21 | Schaffer 4 | $[-100.0,100.0]^{n}$ | 0 | 4 | 1 | 0 |
| F22 | Schaffer 6 | $[-100.0,100.0]^{n}$ | 0 | 6 | 1 | 0 |
| F23 | SixHumpCamelBack | $[-5,5]$ | $[-100.0,100.0]^{n}$ | 0 | 2 | 1 |
| F24 | Bohachevsky 2 | $[-100.0,100.0]^{n}$ | 0 | 3 | 1 | 1 |
| F25 | Bohachevsky 3 | $[-10.0,10.0]^{n}$ | -186.73 | 5 | 1 | 1 |
| F26 | Shubert | $[-5.12,5.12]^{n}$ | -1 | 2 | 0 | 1 |
| F27 | Drop Wave | $[-6.0,6.0]^{n}$ | 0 | 2 | 0 | 0 |
| F28 | Rosenbrock | $[-600.0,600.0]^{n}$ | 0 | 30 | 1 | 0 |
| F29 | Griewank | Ackley | -1.0316 | 2 | 1 | 1 |
| F30 |  | 0 | 2 | 1 | 0 |  |

## C. Benchmark - Unimodal and Separable Functions

To tighten the competitiveness, we identified the algorithms with the highest performances with a t -value above 0.05 . OMOA and A3 (all best solutions in BOLD font) lead with equal best performance as shown in Table IV. The MS was next, followed by A1, HHO, and WFS.

OMOA and A3 leading showed good exploration, and exploitation strength, particularly of OMOA obtained the best optimal objective solutions before the completion of generations. Fig. 10 also shows consistent distributions with fewer outliers.


Fig. 10. Boxplot for unimodal and separable functions.


Fig. 11. Comparison of convergence curve for unimodal and separable functions.

Fig. 11 convergence comparison shows that OMOA, A3, A2, and WFS have faster and best convergences to the optimum in these problems while HHO lagged behind most of the time.

## D. Unimodal and Non-Separable

The functions in this category include 30-dimensional problems Zakharov to Dixon Price with great complexity. Table V shows OMOA and A3 tops, followed by A2, A1, HHO, MS, and WFS. Besides Beale, which did not yield a better result, OMOA got even Easom, a problem with inherent complex nature.

TABLE IV. Unimodal and Separable Functions Results

| F(n) | Measure | OMOA | HHO | MS | EHO | A2 | A3 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F1 | Best | $0.0 \mathrm{E}+00$ | $1.3 \mathrm{E}-06$ | $2.3 \mathrm{E}+00$ | $5.5 \mathrm{E}+00$ | $1.5 \mathrm{E}-01$ | 0.0E+00 |
| $\mathrm{n}=30$ | Worst | 0.0E+00 | 7.6E-05 | $3.7 \mathrm{E}+00$ | $6.4 \mathrm{E}+00$ | 8.5E-01 | 0.0E+00 |
| $\mathrm{f}=0$ | Mean | $0.0 \mathrm{E}+00$ | $2.2 \mathrm{E}-05$ | $3.0 \mathrm{E}+00$ | $6.1 \mathrm{E}+00$ | 4.1E-01 | 0.0E+00 |
|  | Sd | $0.0 \mathrm{E}+00$ | $3.0 \mathrm{E}-05$ | $3.1 \mathrm{E}+00$ | $6.1 \mathrm{E}+00$ | $4.3 \mathrm{E}-01$ | $0.0 \mathrm{E}+00$ |
| F2 | Best | 0.0E+00 | $0.0 \mathrm{E}+00$ | 0.0E+00 | 6.7E-01 | $1.6 \mathrm{E}-01$ | $0.0 \mathrm{E}+00$ |
| $\mathrm{n}=30$ | Worst | 0.0E+00 | $1.1 \mathrm{E}-07$ | 0.0E+00 | $1.7 \mathrm{E}+00$ | 7.1E-01 | 0.0E+00 |
| $\mathrm{f}=0$ | Mean | $0.0 \mathrm{E}+00$ | $1.1 \mathrm{E}-08$ | $0.0 \mathrm{E}+00$ | $1.1 \mathrm{E}+00$ | 4.2E-01 | $0.0 \mathrm{E}+00$ |
|  | Sd | 0.0E+00 | $2.7 \mathrm{E}-08$ | 0.0E+00 | $1.2 \mathrm{E}+00$ | 4.1E-01 | 0.0E+00 |
| F3 | Best | 0.0E+00 | 0.0E+00 | $0.0 \mathrm{E}+00$ | $2.2 \mathrm{E}-01$ | $2.5 \mathrm{E}+00$ | 0.0E+00 |
| $\mathbf{n}=30$ | Worst | 0.0E+00 | 1.2E-07 | $7.2 \mathrm{E}-08$ | $2.9 \mathrm{E}-01$ | $1.2 \mathrm{E}+01$ | 0.0E+00 |
| $\mathrm{f}=0$ | Mean | 0.0E+00 | 6.4E-09 | $4.3 \mathrm{E}-08$ | $2.5 \mathrm{E}-01$ | $6.3 \mathrm{E}+00$ | 0.0E+00 |
|  | Sd | 0.0E+00 | 2.4E-08 | 5.3E-08 | $2.5 \mathrm{E}-01$ | $6.7 \mathrm{E}+00$ | 0.0E+00 |
| F4 | Best | 0.0E+00 | 0.0E+00 | $\mathbf{0 . 0 E + 0 0}$ | $1.2 \mathrm{E}-06$ | $2.1 \mathrm{E}-01$ | 0.0E+00 |
| n=30 | Worst | 0.0E+00 | $0.0 \mathrm{E}+00$ | 0.0E+00 | 2.2E-06 | $5.0 \mathrm{E}+00$ | 0.0E+00 |
| $\mathrm{f}=0$ | Mean | 0.0E+00 | $0.0 \mathrm{E}+00$ | 0.0E+00 | $1.6 \mathrm{E}-06$ | $1.3 \mathrm{E}+00$ | 0.0E+00 |
|  | Sd | 0.0E+00 | 0.0E+00 | 0.0E+00 | 1.6E-06 | $1.5 \mathrm{E}+00$ | 0.0E+00 |

TABLE V. Unimodal and Non-Separable Results for Tested Algorithms

| Function | Measure | OMOA | HHO | MS | EHO | A2 | A3 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F5 | Best | $5.7 \mathrm{E}-07$ | $0.0 \mathrm{E}+00$ | $6.0 \mathrm{E}-05$ | $1.1 \mathrm{E}-05$ | $0.0 \mathrm{E}+00$ | 0.0E+00 |
| $\mathrm{n}=2$ | Worst | $1.7 \mathrm{E}-01$ | 0.0E+00 | 7.2E-04 | 2.3E-02 | $1.5 \mathrm{E}-05$ | 0.0E+00 |
| $\mathrm{f}=0$ | Mean | 4.7E-02 | 0.0E+00 | $2.9 \mathrm{E}-04$ | 7.9E-03 | $1.0 \mathrm{E}-06$ | 0.0E+00 |
|  | Sd | 4.8E-02 | 0.0E+00 | 4.2E-04 | 1.3E-02 | 2.9E-06 | 0.0E+00 |
| F6 | Best | -9.6E-01 | $0.0 \mathrm{E}+00$ | 7.7E-04 | $1.2 \mathrm{E}-01$ | $0.0 \mathrm{E}+00$ | $0.0 \mathrm{E}+00$ |
| $\mathrm{n}=2$ | Worst | -1.7E-235 | $1.9 \mathrm{E}-05$ | $1.3 \mathrm{E}-03$ | 5.7E-01 | $0.0 \mathrm{E}+00$ | $0.0 \mathrm{E}+00$ |
| $\mathrm{f}=\mathbf{- 1}$ | Mean | -3.1E-01 | $1.1 \mathrm{E}-06$ | $1.0 \mathrm{E}-03$ | 3.8E-01 | $0.0 \mathrm{E}+00$ | $0.0 \mathrm{E}+00$ |
|  | Sd | 3.6E-01 | 3.6E-06 | 1.1E-03 | 4.2E-01 | $0.0 \mathrm{E}+00$ | $0.0 \mathrm{E}+00$ |
| F7 | Best | 0.0E+00 | $0.0 \mathrm{E}+00$ | 0.0E+00 | 4.3E-07 | $0.0 \mathrm{E}+00$ | 0.0E+00 |
| $\mathrm{n}=2$ | Worst | 0.0E+00 | 0.0E+00 | 0.0E+00 | 3.0E-06 | 0.0E+00 | 0.0E+00 |
| $\mathrm{f}=0$ | Mean | 0.0E+00 | $0.0 \mathrm{E}+00$ | 0.0E+00 | 1.9E-06 | 0.0E+00 | 0.0E+00 |
|  | Sd | 0.0E+00 | 0.0E+00 | 0.0E+00 | 2.2E-06 | $0.0 \mathrm{E}+00$ | 0.0E+00 |
| F8 | Best | 0.0E+00 | 1.6E-06 | 1.8E-01 | $1.1 \mathrm{E}+00$ | 0.0E+00 | 0.0E+00 |
| $\mathrm{n}=4$ | Worst | 0.0E+00 | 7.7E-01 | $2.9 \mathrm{E}-01$ | $3.2 \mathrm{E}+00$ | 0.0E+00 | 0.0E+00 |
| $\mathrm{f}=0$ | Mean | 0.0E+00 | 3.4E-02 | 2.4E-01 | $1.9 \mathrm{E}+00$ | 0.0E+00 | 0.0E+00 |
|  | Sd | 0.0E+00 | 1.4E-01 | 2.4E-01 | $2.1 \mathrm{E}+00$ | 0.0E+00 | 0.0E+00 |
| F9 | Best | 0.0E+00 | $0.0 \mathrm{E}+00$ | 0.0E+00 | 3.6E-02 | 0.0E+00 | 0.0E+00 |
| $\mathbf{n}=30$ | Worst | 0.0E+00 | 7.7E-07 | 1.3E-08 | $9.1 \mathrm{E}-02$ | 5.1E-08 | 0.0E+00 |
| $\mathrm{f}=0$ | Mean | 0.0E+00 | 8.0E-08 | 4.3E-09 | 6.0E-02 | $1.4 \mathrm{E}-08$ | 0.0E+00 |
|  | Sd | 0.0E+00 | $1.8 \mathrm{E}-07$ | 7.4E-09 | 6.4E-02 | 2.1E-08 | 0.0E+00 |
| F10 | Best | $0.0 \mathrm{E}+00$ | 4.3E-07 | 3.4E-05 | 4.8E-01 | 6.4E-03 | 8.7E-06 |
| $\mathbf{n}=30$ | Worst | 0.0E+00 | $2.7 \mathrm{E}-04$ | 4.6E-04 | 6.2E-01 | 2.7E-02 | 4.3E-05 |
| $\mathrm{f}=0$ | Mean | 0.0E+00 | 4.7E-05 | $1.9 \mathrm{E}-04$ | 5.4E-01 | $1.8 \mathrm{E}-02$ | $1.8 \mathrm{E}-05$ |
|  | Sd | 0.0E+00 | 7.6E-05 | $2.7 \mathrm{E}-04$ | 5.5E-01 | $1.9 \mathrm{E}-02$ | 2.1E-05 |
| F11 | Best | $0.0 \mathrm{E}+00$ | $0.0 \mathrm{E}+00$ | $8.0 \mathrm{E}-08$ | $3.4 \mathrm{E}+00$ | 8.2E-02 | 0.0E+00 |
| $\mathrm{n}=30$ | Worst | 0.0E+00 | $1.9 \mathrm{E}-03$ | $3.8 \mathrm{E}-07$ | 4.2E+00 | $5.5 \mathrm{E}-01$ | 0.0E+00 |
| $\mathrm{f}=0$ | Mean | 0.0E+00 | $9.4 \mathrm{E}-05$ | $2.7 \mathrm{E}-07$ | $3.8 \mathrm{E}+00$ | $3.0 \mathrm{E}-01$ | 0.0E+00 |
|  | Sd | 0.0E+00 | 3.6E-04 | $3.0 \mathrm{E}-07$ | $3.8 \mathrm{E}+00$ | 3.4E-01 | 0.0E+00 |
| F12 | Best | 3.1E-09 | 8.6E-02 | 6.7E-01 | $1.1 \mathrm{E}+00$ | 6.7E-01 | $6.7 \mathrm{E}-01$ |
| $\mathrm{n}=30$ | Worst | 6.7E-04 | 2.6E-01 | 7.0E-01 | $1.3 \mathrm{E}+00$ | 6.7E-01 | 6.7E-01 |
| $\mathbf{f}=0$ | Mean | 3.0E-05 | $2.4 \mathrm{E}-01$ | $6.9 \mathrm{E}-01$ | $1.2 \mathrm{E}+00$ | $6.7 \mathrm{E}-01$ | $6.7 \mathrm{E}-01$ |
|  | Sd | 1.2E-04 | $2.4 \mathrm{E}-01$ | $6.9 \mathrm{E}-01$ | $1.2 \mathrm{E}+00$ | $6.7 \mathrm{E}-01$ | $6.7 \mathrm{E}-01$ |



Fig. 12. Boxplot of unimodal and non-separable results.
The boxplot of Fig. 12 shows that the mean solutions distribution of the data of OMOA and A3 are tight, with little outliers equalling minimal deviation.

The convergence comparison of Fig. 13 confirms the summary made at the beginning of the subsection.


Fig. 13. Comparison of convergence curves for unimodal and non-separable function.

## E. Multimodal and Separable

Complex structures, multiple, unequal hilltops, and valleys-shaped functions are tested as shown in Table VI. Besides the booth function, OMOA had remarkable exploratory abilities for the dimensionalities above $\mathrm{n}=2$ (i.e., $\mathrm{n}=5,10,30$ ) of the last three functions while tracking deeper than values provided by the global optima in literature for Holder Table, Michalewicz (2, 5, and 10). Rastrigin ( $\mathrm{n}=30$ ) was also explored optimally by OMOA and HHO.

TABLE VI. MULTimODAL AND SEPARABLE RESULTS

| Function | Measure | OMOA | HHO | MS | EHO | A2 | A3 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F13 | Best | $0.0 \mathrm{E}+00$ | 0.0E+00 | 2.8E-08 | $5.4 \mathrm{E}-03$ | 0.0E+00 | 0.0E+00 |
| $\mathrm{n}=2$ | Worst | 0.0E+00 | 2.7E-08 | 2.5E-07 | $1.5 \mathrm{E}-02$ | 0.0E+00 | 0.0E+00 |
| $\mathrm{f}=0$ | Mean | $0.0 \mathrm{E}+00$ | 3.3E-09 | $1.7 \mathrm{E}-07$ | $1.0 \mathrm{E}-02$ | $0.0 \mathrm{E}+00$ | 0.0E+00 |
|  | Sd | 0.0E+00 | 8.5E-09 | $2.0 \mathrm{E}-07$ | $1.1 \mathrm{E}-02$ | 0.0E+00 | 0.0E+00 |
| F14 | Best | 1.1E-04 | $0.0 \mathrm{E}+00$ | 8.7E-06 | $3.8 \mathrm{E}-05$ | 0.0E+00 | 0.0E+00 |
| $\mathrm{n}=2$ | Worst | 2.6E-02 | 4.1E-04 | 4.1E-04 | $3.7 \mathrm{E}-02$ | 0.0E+00 | 0.0E+00 |
| $\mathrm{f}=0$ | Mean | $5.5 \mathrm{E}-03$ | $9.1 \mathrm{E}-05$ | $2.4 \mathrm{E}-04$ | $2.0 \mathrm{E}-02$ | 0.0E+00 | 0.0E+00 |
|  | Sd | 5.9E-03 | $1.5 \mathrm{E}-04$ | $3.0 \mathrm{E}-04$ | $2.6 \mathrm{E}-02$ | $\mathbf{0 . 0 E + 0 0}$ | $\mathbf{0 . 0 E + 0 0}$ |
| F15 | Best | -5.0E+04 | $0.0 \mathrm{E}+00$ | -1.8E+01 | -1.7E+01 | $5.3 \mathrm{E}-06$ | $0.0 \mathrm{E}+00$ |
| $\mathrm{n}=2$ | Worst | -2.5E+04 | $1.3 \mathrm{E}-05$ | -1.1E+01 | -1.1E+01 | $3.4 \mathrm{E}-04$ | $0.0 \mathrm{E}+00$ |
| $\mathrm{f}=\mathbf{- 1 9 . 2 0 8 5}$ | Mean | -3.9E+04 | $1.4 \mathrm{E}-06$ | -1.5E+01 | -1.4E+01 | $1.0 \mathrm{E}-04$ | $0.0 \mathrm{E}+00$ |


|  | Sd | 1.2E+04 | 3.4E-06 | $2.8 \mathrm{E}+00$ | 2.7E+00 | $1.1 \mathrm{E}-04$ | $0.0 \mathrm{E}+00$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F16 | Best | -1.8E+00 | $0.0 \mathrm{E}+00$ | $1.2 \mathrm{E}-03$ | $6.5 \mathrm{E}-03$ | $0.0 \mathrm{E}+00$ | $0.0 \mathrm{E}+00$ |
| $\mathrm{n}=2$ | Worst | -1.7E+00 | $2.3 \mathrm{E}-06$ | $7.4 \mathrm{E}-03$ | $3.0 \mathrm{E}-02$ | $0.0 \mathrm{E}+00$ | $0.0 \mathrm{E}+00$ |
| $\mathrm{f}=-1.8013$ | Mean | -1.8E+00 | $2.9 \mathrm{E}-07$ | $3.3 \mathrm{E}-03$ | $1.7 \mathrm{E}-02$ | $0.0 \mathrm{E}+00$ | $0.0 \mathrm{E}+00$ |
|  | Sd | 1.4E-02 | 5.5E-07 | $4.4 \mathrm{E}-03$ | $2.0 \mathrm{E}-02$ | $0.0 \mathrm{E}+00$ | $0.0 \mathrm{E}+00$ |
| F17 | Best | $-4.0 \mathrm{E}+00$ | $1.5 \mathrm{E}-02$ | $2.4 \mathrm{E}-01$ | $9.0 \mathrm{E}-01$ | $2.6 \mathrm{E}-06$ | $0.0 \mathrm{E}+00$ |
| $\mathrm{n}=5$ | Worst | -2.8E+00 | $1.2 \mathrm{E}+00$ | $1.3 \mathrm{E}+00$ | $1.2 \mathrm{E}+00$ | $1.4 \mathrm{E}-04$ | $4.4 \mathrm{E}-02$ |
| $f=-4.6877$ | Mean | -3.6E+00 | 4.7E-01 | $8.5 \mathrm{E}-01$ | $1.1 \mathrm{E}+00$ | $4.0 \mathrm{E}-05$ | 8.7E-03 |
|  | Sd | 2.8E-01 | $6.1 \mathrm{E}-01$ | $9.6 \mathrm{E}-01$ | $1.1 \mathrm{E}+00$ | $6.1 \mathrm{E}-05$ | $1.8 \mathrm{E}-02$ |
| F18 | Best | $-5.5 \mathrm{E}+00$ | $1.6 \mathrm{E}+00$ | $3.4 \mathrm{E}+00$ | $3.4 \mathrm{E}+00$ | $8.6 \mathrm{E}-01$ | $6.5 \mathrm{E}-01$ |
| $\mathrm{n}=10$ | Worst | $-4.2 \mathrm{E}+00$ | $3.8 \mathrm{E}+00$ | $4.9 \mathrm{E}+00$ | $4.2 \mathrm{E}+00$ | $1.3 \mathrm{E}+00$ | $1.4 \mathrm{E}+00$ |
| $f=-9.6602$ | Mean | -4.7E+00 | $2.9 \mathrm{E}+00$ | $4.2 \mathrm{E}+00$ | $3.9 \mathrm{E}+00$ | $1.1 \mathrm{E}+00$ | $1.1 \mathrm{E}+00$ |
|  | Sd | 3.5E-01 | $2.9 \mathrm{E}+00$ | $4.2 \mathrm{E}+00$ | $4.0 \mathrm{E}+00$ | $1.1 \mathrm{E}+00$ | $1.1 \mathrm{E}+00$ |
| F19 | Best | 0.0E+00 | $0.0 \mathrm{E}+00$ | $0.0 \mathrm{E}+00$ | 8.3E-01 | $9.2 \mathrm{E}+01$ | $1.5 \mathrm{E}+01$ |
| $\mathrm{n}=30$ | Worst | $0.0 \mathrm{E}+00$ | $3.3 \mathrm{E}-07$ | 2.2E-07 | $1.2 \mathrm{E}+00$ | $1.1 \mathrm{E}+02$ | $7.3 \mathrm{E}+01$ |
| $\mathbf{f}=\mathbf{0}$ | Mean | 0.0E+00 | $2.1 \mathrm{E}-08$ | $1.2 \mathrm{E}-07$ | $1.0 \mathrm{E}+00$ | $1.0 \mathrm{E}+02$ | $3.5 \mathrm{E}+01$ |
|  | Sd | 0.0E+00 | $6.5 \mathrm{E}-08$ | $1.5 \mathrm{E}-07$ | $1.0 \mathrm{E}+00$ | $1.0 \mathrm{E}+02$ | $3.9 \mathrm{E}+01$ |



Fig. 14. Multimodal and separable boxplot.
The visuals of the boxplot in Fig. 14 show mean solutions of OMOA adequately located in the region with very few deviations and outliers.


Fig. 15. Convergence curves for multimodal and separable function.
In Fig. 15, OMOA had made extra-advance to explore for solutions far better than all the compared algorithms in these problems. Even some of the solutions were far better optimum that set global values as the Holder Table model.

## F. Multimodal and Non-Separable

Table VII shows OMOA led the exploration alongside A3, A2, and HHO though the depth of the troughs in Six-Hump

Camel, Shubert, and Drop Wave seems to have shown that OMOA dived deeper than the others with the peeks of Schaffer 4 also.

TABLE VII. MULTIMODAL AND NON-SEPARABLE RESULTS

| Function | Measure | OMOA | HHO | MS | EHO | A2 | A3 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F20 | Best | 0.0E+00 | $0.0 \mathrm{E}+00$ | $0.0 \mathrm{E}+00$ | 3.3E-07 | 0.0E+00 | $0.0 \mathrm{E}+00$ |
| $\mathrm{n}=2$ | Worst | 4.3E-01 | $0.0 \mathrm{E}+00$ | $0.0 \mathrm{E}+00$ | $6.6 \mathrm{E}-07$ | 0.0E+00 | 0.0E+00 |
| $\mathrm{f}=0$ | Mean | 9.3E-02 | 0.0E+00 | 0.0E+00 | $4.9 \mathrm{E}-07$ | 0.0E+00 | 0.0E+00 |
|  | Sd | 1.2E-01 | $0.0 \mathrm{E}+00$ | $0.0 \mathrm{E}+00$ | 5.1E-07 | 0.0E+00 | $0.0 \mathrm{E}+00$ |
| F21 | Best | 0.0E+00 | 0.0E+00 | 5.8E-08 | 1.3E-06 | 1.0E-08 | $0.0 \mathrm{E}+00$ |
| $\mathrm{n}=4$ | Worst | 1.6E-02 | 1.1E-05 | 7.4E-06 | 1.5E-04 | 2.5E-05 | $0.0 \mathrm{E}+00$ |
| $\mathrm{f}=0.29259$ | Mean | 1.3E-03 | 1.2E-06 | 2.6E-06 | $5.3 \mathrm{E}-05$ | 6.1E-06 | $0.0 \mathrm{E}+00$ |
|  | Sd | 3.7E-03 | 3.2E-06 | 4.3E-06 | $8.7 \mathrm{E}-05$ | 9.3E-06 | 0.0E+00 |
| F22 | Best | 9.7E-03 | $0.0 \mathrm{E}+00$ | $0.0 \mathrm{E}+00$ | $5.2 \mathrm{E}+00$ | $6.7 \mathrm{E}+00$ | $5.5 \mathrm{E}+00$ |
| $\mathrm{n}=6$ | Worst | 4.0E-01 | $2.3 \mathrm{E}-03$ | $2.2 \mathrm{E}-08$ | $6.1 \mathrm{E}+00$ | $9.1 \mathrm{E}+00$ | $7.5 \mathrm{E}+00$ |
| $\mathrm{f}=0$ | Mean | $1.7 \mathrm{E}-01$ | $9.0 \mathrm{E}-05$ | 7.3E-09 | $5.7 \mathrm{E}+00$ | $8.1 \mathrm{E}+00$ | $6.6 \mathrm{E}+00$ |
|  | Sd | $1.2 \mathrm{E}-01$ | $4.3 \mathrm{E}-04$ | $1.3 \mathrm{E}-08$ | $5.8 \mathrm{E}+00$ | $8.1 \mathrm{E}+00$ | 6.7E+00 |
| F23 | Best | $-1.0 \mathrm{E}+00$ | $0.0 \mathrm{E}+00$ | $8.6 \mathrm{E}-07$ | $1.7 \mathrm{E}-04$ | $0.0 \mathrm{E}+00$ | $0.0 \mathrm{E}+00$ |
| $\mathrm{n}=2$ | Worst | $-1.0 \mathrm{E}+00$ | $1.7 \mathrm{E}-08$ | $3.4 \mathrm{E}-05$ | $1.9 \mathrm{E}-03$ | $1.1 \mathrm{E}-07$ | $0.0 \mathrm{E}+00$ |
| $\mathrm{f}=\mathbf{- 1 . 0 3 1 6 3}$ | Mean | -1.0E+00 | $2.2 \mathrm{E}-09$ | $1.6 \mathrm{E}-05$ | 8.2E-04 | 3.2E-08 | $0.0 \mathrm{E}+00$ |
|  | Sd | 9.6E-05 | $5.5 \mathrm{E}-09$ | $2.1 \mathrm{E}-05$ | $1.1 \mathrm{E}-03$ | $5.3 \mathrm{E}-08$ | $0.0 \mathrm{E}+00$ |
| F24 | Best | $0.0 \mathrm{E}+00$ | 0.0E+00 | $1.2 \mathrm{E}-08$ | $5.7 \mathrm{E}-03$ | 0.0E+00 | 0.0E+00 |
| $\mathrm{n}=2$ | Worst | 0.0E+00 | 3.3E-07 | $2.1 \mathrm{E}-07$ | $2.8 \mathrm{E}-02$ | $0.0 \mathrm{E}+00$ | $0.0 \mathrm{E}+00$ |
| $\mathrm{f}=0$ | Mean | $0.0 \mathrm{E}+00$ | $2.5 \mathrm{E}-08$ | $1.2 \mathrm{E}-07$ | $1.9 \mathrm{E}-02$ | $0.0 \mathrm{E}+00$ | $0.0 \mathrm{E}+00$ |
|  | Sd | $0.0 \mathrm{E}+00$ | $7.7 \mathrm{E}-08$ | $1.4 \mathrm{E}-07$ | $2.1 \mathrm{E}-02$ | 0.0E+00 | $0.0 \mathrm{E}+00$ |
| F25 | Best | 0.0E+00 | $0.0 \mathrm{E}+00$ | $0.0 \mathrm{E}+00$ | $3.0 \mathrm{E}-03$ | 0.0E+00 | $0.0 \mathrm{E}+00$ |
| $\mathrm{n}=2$ | Worst | 0.0E+00 | $9.0 \mathrm{E}-06$ | $1.4 \mathrm{E}-08$ | $9.5 \mathrm{E}-03$ | 0.0E+00 | 0.0E+00 |
| $\mathrm{f}=0$ | Mean | 0.0E+00 | $6.2 \mathrm{E}-07$ | $4.6 \mathrm{E}-09$ | $7.2 \mathrm{E}-03$ | 0.0E+00 | $0.0 \mathrm{E}+00$ |
|  | $\mathrm{Sd}$ | 0.0E+00 | $1.9 \mathrm{E}-06$ | $8.0 \mathrm{E}-09$ | $7.8 \mathrm{E}-03$ | $0.0 \mathrm{E}+00$ | 0.0E+00 |
| F26 | Best | -1.9E+02 | -9.0E-06 | $1.1 \mathrm{E}-02$ | $2.3 \mathrm{E}-01$ | -6.0E-06 | -9.0E-06 |
| $\mathrm{n}=2$ | Worst | -1.9E+02 | $2.7 \mathrm{E}-04$ | $3.2 \mathrm{E}-02$ | $1.8 \mathrm{E}+00$ | 8.2E-02 | -9.0E-06 |
| $\mathrm{f}=\mathbf{- 1 8 6 . 7 3}$ | Mean | -1.9E+02 | $2.4 \mathrm{E}-05$ | $2.2 \mathrm{E}-02$ | $1.2 \mathrm{E}+00$ | 2.8E-02 | -9.0E-06 |
|  | Sd | 9.3E-02 | $6.5 \mathrm{E}-05$ | $2.3 \mathrm{E}-02$ | $1.4 \mathrm{E}+00$ | 4.0E-02 | 0.0E+00 |
| F27 | Best | $-1.0 \mathrm{E}+00$ | $0.0 \mathrm{E}+00$ | $0.0 \mathrm{E}+00$ | $3.9 \mathrm{E}-06$ | $0.0 \mathrm{E}+00$ | $0.0 \mathrm{E}+00$ |
| $\mathrm{n}=2$ | Worst | $-1.0 \mathrm{E}+00$ | $0.0 \mathrm{E}+00$ | $1.8 \mathrm{E}-07$ | $3.8 \mathrm{E}-05$ | $0.0 \mathrm{E}+00$ | $0.0 \mathrm{E}+00$ |
| $\mathrm{f}=-1$ | Mean | -1.0E+00 | $0.0 \mathrm{E}+00$ | $6.6 \mathrm{E}-08$ | $2.6 \mathrm{E}-05$ | $0.0 \mathrm{E}+00$ | $0.0 \mathrm{E}+00$ |
|  | Sd | 0.0E+00 | $0.0 \mathrm{E}+00$ | $1.1 \mathrm{E}-07$ | $3.0 \mathrm{E}-05$ | $0.0 \mathrm{E}+00$ | $0.0 \mathrm{E}+00$ |
| F28 | Best | $2.9 \mathrm{E}+01$ | $1.1 \mathrm{E}-03$ | $2.9 \mathrm{E}+01$ | $3.8 \mathrm{E}+01$ | $2.7 \mathrm{E}+01$ | $\mathbf{0 . 0 E + 0 0}$ |
| n $=30$ | Worst | $2.9 \mathrm{E}+01$ | $2.5 \mathrm{E}-01$ | $2.9 \mathrm{E}+01$ | $4.0 \mathrm{E}+01$ | $2.8 \mathrm{E}+01$ | $4.0 \mathrm{E}+00$ |
| $\mathrm{f}=0$ | Mean | $2.9 \mathrm{E}+01$ | $4.5 \mathrm{E}-02$ | $2.9 \mathrm{E}+01$ | $3.9 \mathrm{E}+01$ | $2.8 \mathrm{E}+01$ | $1.2 \mathrm{E}+00$ |
|  | Sd | $9.0 \mathrm{E}-02$ | $7.1 \mathrm{E}-02$ | $2.9 \mathrm{E}+01$ | $3.9 \mathrm{E}+01$ | $2.8 \mathrm{E}+01$ | $2.2 \mathrm{E}+00$ |
| F29 | Best | 0.0E+00 | $0.0 \mathrm{E}+00$ | $0.0 \mathrm{E}+00$ | $9.3 \mathrm{E}-01$ | $6.1 \mathrm{E}-04$ | 0.0E+00 |
| $\mathrm{n}=30$ | Worst | 0.0E+00 | $1.1 \mathrm{E}-06$ | $2.2 \mathrm{E}-08$ | $1.0 \mathrm{E}+00$ | 2.2E-03 | $0.0 \mathrm{E}+00$ |
| $\mathrm{f}=0$ | Mean | 0.0E+00 | 6.9E-08 | 7.3E-09 | $9.7 \mathrm{E}-01$ | 1.3E-03 | $0.0 \mathrm{E}+00$ |
|  | Sd | 0.0E+00 | $2.1 \mathrm{E}-07$ | $1.3 \mathrm{E}-08$ | $9.8 \mathrm{E}-01$ | $1.4 \mathrm{E}-03$ | $\mathbf{0 . 0 E + 0 0}$ |
| F30 | Best | 8.9E-16 | $1.1 \mathrm{E}-06$ | $1.7 \mathrm{E}-05$ | $4.3 \mathrm{E}-01$ | $3.9 \mathrm{E}-03$ | $1.9 \mathrm{E}-06$ |
| n = 30 | Worst | 8.9E-16 | $1.0 \mathrm{E}-04$ | $3.6 \mathrm{E}-05$ | $5.4 \mathrm{E}-01$ | 6.2E-03 | $1.7 \mathrm{E}+00$ |
| $\mathrm{f}=0$ | Mean | 8.9E-16 | $1.8 \mathrm{E}-05$ | $2.4 \mathrm{E}-05$ | $4.8 \mathrm{E}-01$ | $5.0 \mathrm{E}-03$ | 7.2E-01 |
|  | Sd | 8.9E-16 | $2.7 \mathrm{E}-05$ | $2.5 \mathrm{E}-05$ | $4.9 \mathrm{E}-01$ | $5.0 \mathrm{E}-03$ | $9.0 \mathrm{E}-01$ |



Fig. 16. Multimodal and non-separable boxplot.
The boxplot in Fig. 16 shows the clear visuals, confirms OMOA better. The exploratory ability of the OMOA is evident from mean solutions distribution and standard deviations.

The convergence is a reflection of the ability of the tree depth of the network of markets embedded in the model visualized in Fig. 17.


Fig. 17. Convergence curves for multimodal and non-separable function.

## G. Statistical Test and Significance

Table VIII presents the entire statistical hypothesis test carried out to confirm the difference in mean and significance validation in the distribution of solutions by the algorithms on the 30 unconstraint benchmark functions.

Table IX is the summary of the test conducted to prove the hypothesis of the performances of the experiment; 1: means OMOA (in black ink) is more significant, -1: gives better significance to the contender (another algorithm), while $\mathbf{0}$ : depicts no significant difference in performance (contender, equal, OMOA).
table ViII. T-Test for Performance and Hypothesis

| $\begin{aligned} & \mathbf{S} / \\ & \mathbf{N} \end{aligned}$ | Algorithm/ Function | HHO |  |  | MS |  |  | EHO |  |  | A2 |  |  | A3 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | t-value | p-value | $\begin{gathered} \mathrm{Sig} \\ \mathrm{n} \\ \hline \end{gathered}$ | t-value | p-value | $\begin{gathered} \mathrm{Sig} \\ \mathrm{n} \\ \hline \end{gathered}$ | t-value | p-value | $\begin{gathered} \mathrm{Sig} \\ \mathrm{n} \\ \hline \end{gathered}$ | t-value | p-value | $\begin{gathered} \mathrm{Sig} \\ \mathrm{n} \\ \hline \end{gathered}$ | t-value | p-value | $\overline{\mathrm{Sig}}$ |
| 1 | Step | $5.8 \mathrm{E}+00$ | 2.5E-06 | 1 | $2.8 \mathrm{E}+01$ | 2.1E-22 | 1 | $7.5 \mathrm{E}+01$ | 8.7E-35 | 1 | $1.3 \mathrm{E}+01$ | 8.9E-14 | 1 | nan | nan | 0 |
| 2 | Sphere | $2.3 \mathrm{E}+00$ | 3.1E-02 | 1 | nan | nan | 0 | $1.4 \mathrm{E}+01$ | $9.6 \mathrm{E}-15$ | 1 | $1.5 \mathrm{E}+01$ | 5.4E-15 | 1 | nan | nan | 0 |
| 3 | SumSquare | $1.5 \mathrm{E}+00$ | $1.4 \mathrm{E}-01$ | 1 | $7.5 \mathrm{E}+00$ | 2.8E-08 | 1 | $4.5 \mathrm{E}+01$ | 2.4E-28 | 1 | $1.4 \mathrm{E}+01$ | $1.0 \mathrm{E}-14$ | 1 | nan | nan | 0 |
| 4 | Quartic | nan | nan | 0 | nan | nan | 0 | $2.0 \mathrm{E}+01$ | 1.9E-18 | 1 | $9.7 \mathrm{E}+00$ | 1.4E-10 | 1 | nan | nan | 0 |
| 5 | Beale | $5.3 \mathrm{E}+00$ | $9.9 \mathrm{E}-06$ | -1 | $5.3 \mathrm{E}+00$ | $1.1 \mathrm{E}-05$ | -1 | $4.1 \mathrm{E}+00$ | 3.3E-04 | -1 | $5.3 \mathrm{E}+00$ | $9.9 \mathrm{E}-06$ | 1 | 5.3E+00 | $9.9 \mathrm{E}-06$ | -1 |
| 6 | Easom | $4.6 \mathrm{E}+00$ | 7.5E-05 | 1 | $4.6 \mathrm{E}+00$ | 7.2E-05 | 1 | $8.0 \mathrm{E}+00$ | 9.1E-09 | 1 | $4.6 \mathrm{E}+00$ | 7.5E-05 | 1 | $4.6 \mathrm{E}+00$ | 7.5E-05 | 1 |
| 7 | Matyas | nan | nan | 0 | nan | nan | 0 | $9.4 \mathrm{E}+00$ | 2.6E-10 | 1 | nan | nan | 0 | nan | nan | 0 |
| 8 | Colville | $5.3 \mathrm{E}+00$ | 1.1E-05 | 1 | $5.1 \mathrm{E}+00$ | 2.0E-05 | 1 | $3.0 \mathrm{E}+01$ | 1.7E-23 | 1 | nan | nan | 0 | nan | nan | 0 |
| 9 | Zakharov | $2.7 \mathrm{E}+00$ | 1.3E-02 | 1 | $3.8 \mathrm{E}+00$ | 6.7E-04 | 1 | $1.4 \mathrm{E}+01$ | 4.0E-14 | 1 | $4.4 \mathrm{E}+00$ | 1.3E-04 | 1 | nan | nan | 0 |
| 10 | $\begin{aligned} & \hline \text { Schwefel } \\ & 2.22 \\ & \hline \end{aligned}$ | $4.2 \mathrm{E}+00$ | $2.4 \mathrm{E}-04$ | 1 | $5.3 \mathrm{E}+00$ | 1.1E-05 | 1 | $4.8 \mathrm{E}+01$ | 2.7E-29 | 1 | $1.7 \mathrm{E}+01$ | 2.7E-16 | 1 | $9.9 \mathrm{E}+00$ | $9.2 \mathrm{E}-11$ | 1 |
| 11 | Schwefel $1.2$ | $\begin{aligned} & \hline- \\ & 1.4 \mathrm{E}+00 \\ & \hline \end{aligned}$ | 1.6E-01 | 0 | $1.1 \mathrm{E}+01$ | 1.2E-11 | 1 | $6.1 \mathrm{E}+01$ | 3.0E-32 | 1 | $1.1 \mathrm{E}+01$ | 2.3E-11 | 1 | nan | nan | 0 |
| 12 | Dixon Price | $3.6 \mathrm{E}+01$ | 1.0E-25 | 1 | $2.7 \mathrm{E}+02$ | 1.3E-50 | 1 | $8.1 \mathrm{E}+01$ | 1.1E-35 | 1 | $1.1 \mathrm{E}+04$ | 7.8E-98 | 1 | $3.0 \mathrm{E}+04$ | $\begin{aligned} & \hline 3.3 \mathrm{E}- \\ & 110 \\ & \hline \end{aligned}$ | 1 |
| 13 | $\begin{aligned} & \hline \text { Bohachevsk } \\ & \text { y } 1 \\ & \hline \end{aligned}$ | $2.2 \mathrm{E}+00$ | 3.3E-02 | 1 | $9.1 \mathrm{E}+00$ | 5.5E-10 | 1 | $1.3 \mathrm{E}+01$ | 9.3E-14 | 1 | nan | nan | 0 | nan | nan | 0 |
| 14 | Booth | 5.1E+00 | $2.1 \mathrm{E}-05$ | -1 | $4.9 \mathrm{E}+00$ | $3.4 \mathrm{E}-05$ | -1 | $5.5 \mathrm{E}+00$ | 7.3E-06 | 1 | 5.2E+00 | 1.6E-05 | -1 | 5.2E+00 | $1.6 \mathrm{E}-05$ | -1 |
| 15 | Holder Table | $1.8 \mathrm{E}+01$ | 2.1E-17 | 1 | $1.8 \mathrm{E}+01$ | 2.1E-17 | 1 | $1.8 \mathrm{E}+01$ | 2.1E-17 | 1 | $1.8 \mathrm{E}+01$ | 2.1E-17 | 1 | $1.8 \mathrm{E}+01$ | $2.1 \mathrm{E}-17$ | 1 |
| 16 | Michalewic z 2 | $7.1 \mathrm{E}+02$ | 5.9E-63 | 1 | $6.8 \mathrm{E}+02$ | 2.0E-62 | 1 | $1.4 \mathrm{E}-59$ | 1.3E-53 | -1 | 7.1E+02 | 5.9E-63 | 1 | $7.1 \mathrm{E}+02$ | 5.9E-63 | 1 |
| 17 | Michalewic z 5 | $4.5 \mathrm{E}+01$ | 1.9E-28 | 1 | $4.8 \mathrm{E}+01$ | 2.9E-29 | 1 | $7.5 \mathrm{E}+01$ | 9.8E-35 | 1 | $6.9 \mathrm{E}+01$ | $9.8 \mathrm{E}-34$ | 1 | 7.1E+01 | 4.4E-34 | 1 |
| 18 | $\begin{aligned} & \text { Michalewic } \\ & \text { z } 10 \\ & \hline \end{aligned}$ | $6.7 \mathrm{E}+01$ | $2.9 \mathrm{E}-33$ | 1 | $6.6 \mathrm{E}+01$ | 4.2E-33 | 1 | $9.5 \mathrm{E}+01$ | 9.2E-38 | 1 | $8.0 \mathrm{E}+01$ | 1.4E-35 | 1 | $7.5 \mathrm{E}+01$ | 1.0E-34 | 1 |
| 19 | Rastrigin | $1.9 \mathrm{E}+00$ | 7.1E-02 | 0 | $6.9 \mathrm{E}+00$ | 1.2E-07 | 1 | $4.0 \mathrm{E}+01$ | 5.0E-27 | 1 | $9.5 \mathrm{E}+01$ | 9.4E-38 | 1 | $1.0 \mathrm{E}+01$ | 3.2E-11 | 1 |
| 20 | Schaffer 2 | $4.1 \mathrm{E}+00$ | 3.1E-04 | -1 | $4.1 \mathrm{E}+00$ | 3.1E-04 | -1 | 4.1E+00 | 3.1E-04 | -1 | 4.1E+00 | 3.1E-04 | -1 | 4.1E+00 | 3.1E-04 | -1 |
| 21 | Schaffer 4 | $1.4 \mathrm{E}+00$ | $1.7 \mathrm{E}-01$ | 0 | $1.9 \mathrm{E}+00$ | 6.7E-02 | 0 | $1.8 \mathrm{E}+00$ | 7.8E-02 | 0 | $1.9 \mathrm{E}+00$ | 6.8E-02 | 0 | $1.9 \mathrm{E}+00$ | $6.6 \mathrm{E}-02$ | 0 |
| 22 | Schaffer 6 | $7.8 \mathrm{E}+00$ | $1.3 \mathrm{E}-08$ | -1 | $7.8 \mathrm{E}+00$ | 1.2E-08 | -1 | $6.4 \mathrm{E}+01$ | 9.9E-33 | 1 | $6.6 \mathrm{E}+01$ | 3.1E-33 | 1 | $5.0 \mathrm{E}+01$ | 8.9E-30 | 1 |
| 23 | 6HumCame 1 Back | $5.9 \mathrm{E}+04$ | $\begin{aligned} & \hline 1.0 \mathrm{E}- \\ & 118 \\ & \hline \end{aligned}$ | 1 | $6.1 \mathrm{E}+04$ | $\begin{aligned} & \text { 3.5E- } \\ & 119 \\ & \hline \end{aligned}$ | 1 | $7.3 \mathrm{E}+03$ | 2.6E-92 | 1 | $5.9 \mathrm{E}+04$ | $\begin{aligned} & \hline 1.0 \mathrm{E}- \\ & 118 \\ & \hline \end{aligned}$ | 1 | $5.9 \mathrm{E}+04$ | $\begin{aligned} & \hline 1.0 \mathrm{E}- \\ & 118 \\ & \hline \end{aligned}$ | 1 |
| 24 | Bohachevsk $\mathrm{y} 2$ | $1.8 \mathrm{E}+00$ | 7.8E-02 | 0 | $7.8 \mathrm{E}+00$ | 1.3E-08 | 1 | $1.1 \mathrm{E}+01$ | 1.5E-11 | 1 | nan | nan | 0 | nan | nan | 0 |
| 25 | $\begin{aligned} & \text { Bohachevsk } \\ & \text { y } 3 \end{aligned}$ | $1.9 \mathrm{E}+00$ | 7.0E-02 | 0 | $7.8 \mathrm{E}+00$ | 1.3E-08 | 1 | $3.8 \mathrm{E}+00$ | 6.7E-04 | 1 | nan | nan | 0 | nan | nan | 0 |
| 26 | Shubert | $1.1 \mathrm{E}+04$ | 1.5E-97 | 1 | $1.1 \mathrm{E}+04$ | 2.2E-97 | 1 | $1.4 \mathrm{E}+03$ | 8.3E-72 | 1 | $1.0 \mathrm{E}+04$ | 2.1E-96 | 1 | $1.1 \mathrm{E}+04$ | $1.5 \mathrm{E}-97$ | 1 |
| 27 | Drop Wave | -inf | $0.0 \mathrm{E}+00$ | 1 | $6.6 \mathrm{E}+07$ | $\begin{aligned} & \hline 3.4 \mathrm{E}- \\ & 207 \\ & \hline \end{aligned}$ | 1 | $3.5 \mathrm{E}+05$ | $\begin{aligned} & \hline 5.8 \mathrm{E}- \\ & 141 \\ & \hline \end{aligned}$ | 1 | -inf | $0.0 \mathrm{E}+00$ | 1 | -inf | 0.0E+00 | 1 |
| 28 | Rosenbrock | $1.7 \mathrm{E}+03$ | $9.7 \mathrm{E}-74$ | -1 | $\begin{aligned} & -3.3 \mathrm{E}- \\ & 02 \\ & \hline \end{aligned}$ | 9.7E-01 | 0 | $5.9 \mathrm{E}+01$ | 1.0E-31 | 1 | $2.2 \mathrm{E}+01$ | 1.9E-19 | -1 | 8.2E+01 | 7.4E-36 | -1 |
| 29 | Grienwank | $1.9 \mathrm{E}+00$ | 7.4E-02 | 0 | $3.8 \mathrm{E}+00$ | 6.7E-04 | 1 | $1.4 \mathrm{E}+02$ | 2.2E-42 | 1 | $1.3 \mathrm{E}+01$ | 6.9E-14 | 1 | nan | nan | 0 |
| 30 | Ackley | $4.9 \mathrm{E}+00$ | 3.4E-05 | 1 | $1.5 \mathrm{E}+01$ | 7.1E-15 | 1 | $5.7 \mathrm{E}+01$ | 2.3E-31 | 1 | $3.2 \mathrm{E}+01$ | 3.8E-24 | 1 | $7.2 \mathrm{E}+00$ | 7.0E-08 | 1 |
| Sign (better) ==> Significance ( $1=$ OMOA; -1 = Alternative Algorithm; $0=$ no significant difference), nan $=$ not a number, inf $=$ infinite |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

TABLE IX. Summary of Significance and Rank

| $(-1,0,1)$ | HHO | MS | EHO | A2 | A3 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| OMOA | $[5,8, \mathbf{1 7}]$ | $[4,5,21]$ | $[2,1,27]$ | $[3,6,21]$ | $[4,13,13]$ |

The highest equal performance point, 13 is between OMOA and A3, with OMOA leading with 13 optimal solutions, more than A3's other 4 better performances. Next is HHO with 8 equal points, OMOA with 7 better optimal solutions, and HHO making 5 places. MS and A1 shared very close contest with EHO behind. Table X also is the presentation of the mean runtime measure given below.

TABLE X. Runtime Test Results based on Rastrigin

| OMOA | HHO | MS | EHO | A2 | A3 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{2 . 4 9 3 0 9 6}$ | 45.6716 | 756.4435 | 788.1535 | 202.0933 | 217.6285 |

The performance of OMOA in this section was very high on benchmark complex unconstraint problems compared to contending methods.

## H. Results and Statistical Testing with CEC 2017

This section reports OMOA on real-parameter single objective optimization challenging problems featured in Computational Evolution Computation - CEC 2017 with a statistical comparison between OMOA and winners of the competition.

## I. Result of OMOA with CEC 2017

The values are the differences between the global optima and the ones obtained with OMOA for 10D, 30D , and 100D during every 51 runs, as shown in the Table XI, and competition is presented in Table XII for 50D

1) 10D , 30D, 50D and 100D Performances

- The uni-modal functions EC1, EC2, and EC3 results were least expected within the number of functional evaluations provided, perhaps due to parameter tuning differences from recommended.
- EC7 - EC10 multimodal functions all attained global optima in all dimensions. OMOA also met 10D and 30D optimal values, with a minor difference for 50D and not too good 100D. EC5 solutions are not good in all dimensions; while EC6 10D was globally optimal, the rest dimensions were not impressive and inadequate for some ranges of solutions.
- Hybrid functions optimization; OMOA yielded optimal global solutions for EC11, EC14 - EC17, and EC19EC20 leaving out EC12, EC13, and EC18 with not too good in solutions.
- Besides EC21, EC22, and EC27 of the Composition functions with non-optimal solutions, OMOA achieved optimal global solutions for others, i.e., EC23, EC24, EC25, EC26, EC28, and EC29 in all dimensions, respectively.


## J. Time Complexity Analysis

The competition provided appropriate information on the modalities to compute the time complexity [39]. The observation and experimentation shown in Table XII of this work is as follows:

- Evaluate a code consisting of basic arithmetic operation for $1,000,000$ iterations and recode the time $\left(\mathrm{T}_{0}\right)$.
- Evaluate the hybrid function EC18 for 200,000 times the four dimensions (10D , 30D , 50D, and 100D) with record $\left(\mathrm{T}_{1}\right)$.
- For every dimension, find the meantime of computing $\bar{T}_{2}$ the hybrid function EC18 five times run with a termination iteration of 200,000 .
- Calculate the time complexity of the algorithm using the relation $\left(\bar{T}_{2}-T_{1}\right) / T_{0}$.

Table XIII depicts that the complexity of OMOA is not increasing significantly with the increase in the dimension of the functions.

TABLE XI. Statistical Results For CEC 2017 Simulations D10, D30, and D100

| Tag | Best |  |  | Worst |  |  | Mean |  |  | Median |  |  | Standard Deviation |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Tag | 10D | 30D | 100D | 10D | 30D | 100D | 10D | 30D | 100D | 10D | 30D | 100D | 10D | 30D | 100D |
| $\begin{aligned} & \hline \mathrm{EC} \\ & 1 \\ & \hline \end{aligned}$ | $3.6 \mathrm{E}+3$ | 6.3E+4 | 5.8E+5 | 1.7E+4 | 1.3E+5 | $1.7 \mathrm{E}+6$ | 1.1E+4 | $9.9 \mathrm{E}+4$ | $1.1 \mathrm{E}+6$ | 1.1E+4 | $1.0 \mathrm{E}+5$ | $1.1 \mathrm{E}+6$ | $\begin{aligned} & 3.1 \mathrm{E}+ \\ & 3 \\ & \hline \end{aligned}$ | $1.6 \mathrm{E}+4$ | 2.7E+5 |
| $\begin{aligned} & \hline \text { EC } \\ & 2 \\ & \hline \end{aligned}$ | $3.6 \mathrm{E}+3$ | 6.3E+4 | $\begin{aligned} & \hline 5.8 \mathrm{E}+0 \\ & 5 \\ & \hline \end{aligned}$ | 1.7E+4 | $\begin{aligned} & 1.3 \mathrm{E}+0 \\ & 5 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 1.7 \mathrm{E}+00 \\ & 6 \\ & \hline \end{aligned}$ | $1.1 \mathrm{E}+4$ | $\begin{aligned} & 9.9 \mathrm{E}+0 \\ & 4 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.1 \mathrm{E}+00 \\ & 6 \\ & \hline \end{aligned}$ | 1.1E+4 | $\begin{aligned} & 1.0 \mathrm{E}+0 \\ & 5 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.1 \mathrm{E}+0 \\ & 6 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 3.1 \mathrm{E}+ \\ & 3 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.6 \mathrm{E}+0 \\ & 4 \end{aligned}$ | $\begin{aligned} & 2.7 \mathrm{E}+0 \\ & 5 \\ & \hline \end{aligned}$ |
| $\begin{aligned} & \hline \text { EC } \\ & 3 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.9 \mathrm{E}+0 \\ & 3 \\ & \hline \end{aligned}$ | 7.3E+4 | 7.9E+5 | 1.8E+4 | 1.9E+5 | $1.8 \mathrm{E}+6$ | $9.0 \mathrm{E}+3$ | 1.3E+5 | $1.4 \mathrm{E}+6$ | $8.9 \mathrm{E}+3$ | $1.3 \mathrm{E}+5$ | $1.4 \mathrm{E}+6$ | $\begin{aligned} & 3.5 \mathrm{E}+ \\ & 3 \\ & \hline \end{aligned}$ | 3.1E+4 | $2.5 \mathrm{E}+5$ |
| $\begin{aligned} & \hline \mathrm{EC} \\ & 4 \\ & \hline \end{aligned}$ | 0.0E+0 | 0.0E+0 | $1.9 \mathrm{E}+3$ | $0.0 \mathrm{E}+0$ | 0.0E+0 | $2.5 \mathrm{E}+3$ | 0.0E+0 | 0.0E+0 | $2.3 \mathrm{E}+3$ | 0.0E+0 | $0.0 \mathrm{E}+0$ | $2.3 \mathrm{E}+3$ | $\begin{aligned} & \hline 0.0 \mathrm{E}+ \\ & 0 \\ & \hline \end{aligned}$ | 0.0E+0 | 1.4E+2 |
| $\begin{aligned} & \text { EC } \\ & 5 \end{aligned}$ | $1.5 \mathrm{E}+7$ | $4.0 \mathrm{E}+7$ | $1.2 \mathrm{E}+8$ | $1.5 \mathrm{E}+7$ | $4.0 \mathrm{E}+7$ | $1.2 \mathrm{E}+8$ | $1.5 \mathrm{E}+7$ | $4.0 \mathrm{E}+7$ | $1.2 \mathrm{E}+8$ | 1.5E+7 | $4.0 \mathrm{E}+7$ | $1.2 \mathrm{E}+8$ | $\begin{aligned} & \text { 0.0E+ } \\ & 0 \end{aligned}$ | 0.0E+0 | 0.0E+0 |
| $\begin{aligned} & \hline \text { EC } \\ & 6 \\ & \hline \end{aligned}$ | 0.0E+0 | 4.4E+2 | $9.0 \mathrm{E}+3$ | $0.0 \mathrm{E}+0$ | $1.8 \mathrm{E}+3$ | $1.2 \mathrm{E}+4$ | 0.0E+0 | $1.3 \mathrm{E}+3$ | $1.1 \mathrm{E}+4$ | 0.0E+0 | $1.3 \mathrm{E}+3$ | $1.1 \mathrm{E}+4$ | $\begin{aligned} & \text { 0.0E+ } \\ & 0 \end{aligned}$ | $2.9 \mathrm{E}+2$ | 6.6E+2 |
| $\begin{aligned} & \hline \text { EC } \\ & 7 \\ & \hline \end{aligned}$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | $\begin{aligned} & 0.0 \mathrm{E}+ \\ & 0 \\ & \hline \end{aligned}$ | 0.0E+0 | 0.0E+0 |
| $\begin{aligned} & \hline \text { EC } \\ & 8 \\ & \hline \end{aligned}$ | 0.0E+0 | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | 0.0E+0 | $0.0 \mathrm{E}+0$ | 0.0E+0 | $0.0 \mathrm{E}+0$ | 0.0E+0 | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | $\begin{aligned} & 0.0 \mathrm{E}+ \\ & 0 \\ & \hline \end{aligned}$ | 0.0E+0 | 0.0E+0 |
| $\begin{aligned} & \hline \text { EC } \\ & 9 \\ & \hline \end{aligned}$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | 0.0E+0 | $0.0 \mathrm{E}+0$ | 0.0E+0 | 0.0E+0 | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | $\begin{aligned} & 0.0 \mathrm{E}+ \\ & 0 \\ & \hline \end{aligned}$ | 0.0E+0 | $0.0 \mathrm{E}+0$ |
| $\begin{aligned} & \hline \text { EC } \\ & 10 \\ & \hline \end{aligned}$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | 0.0E+0 | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | $\begin{aligned} & 0.0 \mathrm{E}+ \\ & 0 \\ & \hline \end{aligned}$ | 0.0E+0 | 0.0E+0 |


| $\begin{aligned} & \hline \text { EC } \\ & 11 \\ & \hline \end{aligned}$ | $0.0 \mathrm{E}+0$ | 0.0E+0 | $0.0 \mathrm{E}+0$ | 0.0E+0 | $0.0 \mathrm{E}+0$ | 0.0E+0 | 0.0E+0 | 0.0E+0 | $0.0 \mathrm{E}+0$ | 0.0E+0 | 0.0E+0 | 0.0E+0 | $\begin{aligned} & \hline 0.0 \mathrm{E}+ \\ & 0 \\ & \hline \end{aligned}$ | 0.0E+0 | $0.0 \mathrm{E}+0$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \hline \text { EC } \\ & 12 \\ & \hline \end{aligned}$ | $3.7 \mathrm{E}+3$ | 4.5E+4 | $2.4 \mathrm{E}+5$ | $1.4 \mathrm{E}+4$ | 7.7E+4 | 3.2E+5 | $8.5 \mathrm{E}+3$ | $6.2 \mathrm{E}+4$ | $3.0 \mathrm{E}+5$ | $8.4 \mathrm{E}+3$ | 6.2E+4 | $3.0 \mathrm{E}+5$ | $\begin{aligned} & 2.6 \mathrm{E}+ \\ & 3 \\ & \hline \end{aligned}$ | $6.5 \mathrm{E}+3$ | $1.5 \mathrm{E}+4$ |
| $\begin{aligned} & \hline \text { EC } \\ & 13 \\ & \hline \end{aligned}$ | $1.6 \mathrm{E}+8$ | $\begin{aligned} & 1.4 \mathrm{E}+1 \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & 4.9 \mathrm{E}+1 \\ & 0 \\ & \hline \end{aligned}$ | $3.7 \mathrm{E}+9$ | $\begin{aligned} & \hline 3.8 \mathrm{E}+1 \\ & 0 \\ & \hline \end{aligned}$ | $9.4 \mathrm{E}+10$ | $1.8 \mathrm{E}+9$ | $\begin{aligned} & 2.8 \mathrm{E}+1 \\ & 0 \\ & \hline \end{aligned}$ | $7.3 \mathrm{E}+10$ | $1.8 \mathrm{E}+9$ | $\begin{aligned} & 2.8 \mathrm{E}+1 \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 7.4 \mathrm{E}+1 \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & 8.3 \mathrm{E}+ \\ & 8 \\ & \hline \end{aligned}$ | $5.6 \mathrm{E}+9$ | $\begin{aligned} & 1.1 \mathrm{E}+1 \\ & 0 \\ & \hline \end{aligned}$ |
| $\begin{aligned} & \text { EC } \\ & 14 \end{aligned}$ | $0.0 \mathrm{E}+0$ | 0.0E+0 | 0.0E+0 | 0.0E+0 | 0.0E+0 | 0.0E+0 | 0.0E+0 | 0.0E+0 | 0.0E+0 | 0.0E+0 | 0.0E+0 | 0.0E+0 | $\begin{aligned} & \hline 0.0 \mathrm{E}+ \\ & 0 \\ & \hline \end{aligned}$ | 0.0E+0 | $0.0 \mathrm{E}+0$ |
| $\begin{aligned} & \mathrm{EC} \\ & 15 \\ & \hline \end{aligned}$ | $0.0 \mathrm{E}+0$ | 0.0E+0 | 0.0E+0 | 0.0E+0 | $0.0 \mathrm{E}+0$ | 0.0E+0 | 0.0E+0 | 0.0E+0 | 0.0E+0 | 0.0E+0 | 0.0E+0 | 0.0E+0 | $\begin{aligned} & \hline 0.0 \mathrm{E}+ \\ & 0 \\ & \hline \end{aligned}$ | 0.0E+0 | $0.0 \mathrm{E}+0$ |
| $\begin{aligned} & \hline \mathrm{EC} \\ & 16 \\ & \hline \end{aligned}$ | $0.0 \mathrm{E}+0$ | 0.0E+0 | $0.0 \mathrm{E}+0$ | 0.0E+0 | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | 0.0E+0 | 0.0E+0 | 0.0E+0 | 0.0E+0 | 0.0E+0 | 0.0E+0 | $\begin{aligned} & \hline 0.0 \mathrm{E}+ \\ & 0 \end{aligned}$ | 0.0E+0 | $0.0 \mathrm{E}+0$ |
| $\begin{aligned} & \hline \text { EC } \\ & 17 \\ & \hline \end{aligned}$ | $0.0 \mathrm{E}+0$ | 0.0E+0 | 0.0E+0 | 0.0E+0 | 0.0E+0 | $0.0 \mathrm{E}+0$ | 0.0E+0 | 0.0E+0 | $0.0 \mathrm{E}+0$ | 0.0E+0 | 0.0E+0 | 0.0E+0 | $\begin{aligned} & 0.0 \mathrm{E}+ \\ & 0 \\ & \hline \end{aligned}$ | 0.0E+0 | $0.0 \mathrm{E}+0$ |
| $\begin{aligned} & \hline \text { EC } \\ & 18 \\ & \hline \end{aligned}$ | $3.8 \mathrm{E}+3$ | 4.6E+4 | $2.4 \mathrm{E}+5$ | 1.4E+4 | 7.7E+4 | 3.2E+5 | $8.5 \mathrm{E}+3$ | 6.2E+4 | $3.0 \mathrm{E}+5$ | 8.3E+3 | 6.2E+4 | $3.0 \mathrm{E}+5$ | $\begin{aligned} & \hline 2.6 \mathrm{E}+ \\ & 3 \\ & \hline \end{aligned}$ | $6.5 \mathrm{E}+3$ | $1.5 \mathrm{E}+4$ |
| $\begin{aligned} & \hline \text { EC } \\ & 19 \\ & \hline \end{aligned}$ | $0.0 \mathrm{E}+0$ | 0.0E+0 | 0.0E+0 | 0.0E+0 | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | 0.0E+0 | 0.0E+0 | 0.0E+0 | 0.0E+0 | 0.0E+0 | $\begin{aligned} & 0.0 \mathrm{E}+ \\ & 0 \\ & \hline \end{aligned}$ | 0.0E+0 | $0.0 \mathrm{E}+0$ |
| $\begin{aligned} & \hline \text { EC } \\ & 20 \\ & \hline \end{aligned}$ | $0.0 \mathrm{E}+0$ | 0.0E+0 | 0.0E+0 | 0.0E+0 | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | 0.0E+0 | 0.0E+0 | 0.0E+0 | 0.0E+0 | 0.0E+0 | 0.0E+0 | $\begin{aligned} & 0.0 \mathrm{E}+ \\ & 0 \\ & \hline \end{aligned}$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ |
| $\begin{aligned} & \hline \text { EC } \\ & 21 \\ & \hline \end{aligned}$ | 1.3E+4 | 1.6E+5 | 7.9E+5 | 4.7E+4 | $2.6 \mathrm{E}+5$ | $1.1 \mathrm{E}+6$ | $2.8 \mathrm{E}+4$ | $2.2 \mathrm{E}+5$ | $1.0 \mathrm{E}+6$ | 2.9E+4 | $2.2 \mathrm{E}+5$ | $1.0 \mathrm{E}+6$ | $\begin{aligned} & 8.0 \mathrm{E}+ \\ & 3 \\ & \hline \end{aligned}$ | $2.6 \mathrm{E}+4$ | 6.8E+4 |
| $\begin{aligned} & \hline \text { EC } \\ & 22 \\ & \hline \end{aligned}$ | 3.6E+9 | $\begin{aligned} & \hline 2.1 \mathrm{E}+1 \\ & 1 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.8 \mathrm{E}+1 \\ & 2 \\ & \hline \end{aligned}$ | $\begin{aligned} & 4.0 \mathrm{E}+1 \\ & 0 \\ & \hline \end{aligned}$ | $6.1 \mathrm{E}+1$ | 3.3E+12 | $\begin{aligned} & 1.6 \mathrm{E}+1 \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 4.0 \mathrm{E}+1 \\ & 1 \\ & \hline \end{aligned}$ | $2.7 \mathrm{E}+12$ | $\begin{aligned} & 1.5 \mathrm{E}+1 \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 3.9 \mathrm{E}+1 \\ & 1 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 2.7 \mathrm{E}+1 \\ & 2 \\ & \hline \end{aligned}$ | $\begin{aligned} & 7.8 \mathrm{E}+ \\ & 9 \\ & \hline \end{aligned}$ | $\begin{aligned} & 9.8 \mathrm{E}+1 \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 3.3 \mathrm{E}+1 \\ & 1 \\ & \hline \end{aligned}$ |
| $\begin{aligned} & \hline \mathrm{EC} \\ & 23 \\ & \hline \end{aligned}$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | 0.0E+0 | 0.0E+0 | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | 0.0E+0 | 0.0E+0 | 0.0E+0 | 0.0E+0 | 0.0E+0 | $\begin{aligned} & 0.0 \mathrm{E}+ \\ & 0 \\ & \hline \end{aligned}$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ |
| $\begin{aligned} & \hline \text { EC } \\ & 24 \\ & \hline \end{aligned}$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | 0.0E+0 | 0.0E+0 | $0.0 \mathrm{E}+0$ | 0.0E+0 | 0.0E+0 | 0.0E+0 | 0.0E+0 | 0.0E+0 | 0.0E+0 | 0.0E+0 | $\begin{aligned} & \hline 0.0 \mathrm{E}+ \\ & 0 \\ & \hline \end{aligned}$ | 0.0E+0 | $0.0 \mathrm{E}+0$ |
| $\begin{aligned} & \hline \text { EC } \\ & 25 \\ & \hline \end{aligned}$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | $5.0 \mathrm{E}+3$ | 0.0E+0 | $0.0 \mathrm{E}+0$ | 6.1E+3 | 0.0E+0 | 0.0E+0 | $5.6 \mathrm{E}+3$ | 0.0E+0 | 0.0E+0 | 5.7E+3 | $\begin{aligned} & \hline 0.0 \mathrm{E}+ \\ & 0 \\ & \hline \end{aligned}$ | 0.0E+0 | $2.9 \mathrm{E}+2$ |
| $\begin{aligned} & \text { EC } \\ & 26 \\ & \hline \end{aligned}$ | 0.0E+0 | 0.0E+0 | 0.0E+0 | 0.0E+0 | $0.0 \mathrm{E}+0$ | 0.0E+0 | 0.0E+0 | 0.0E+0 | 0.0E+0 | 0.0E+0 | 0.0E+0 | 0.0E+0 | $\begin{aligned} & 0.0 \mathrm{E}+ \\ & 0 \\ & \hline \end{aligned}$ | 0.0E+0 | $0.0 \mathrm{E}+0$ |
| $\begin{aligned} & \hline \text { EC } \\ & 27 \\ & \hline \end{aligned}$ | $1.3 \mathrm{E}+4$ | 1.6E+5 | 7.9E+5 | 4.7E+4 | $2.6 \mathrm{E}+5$ | $1.1 \mathrm{E}+6$ | $2.8 \mathrm{E}+4$ | 2.2E+5 | $1.0 \mathrm{E}+6$ | 2.9E+4 | 2.2E+5 | $1.0 \mathrm{E}+6$ | $\begin{aligned} & 8.0 \mathrm{E}+ \\ & 3 \\ & \hline \end{aligned}$ | $2.6 \mathrm{E}+4$ | 6.8E+4 |
| $\begin{aligned} & \hline \text { EC } \\ & 28 \\ & \hline \end{aligned}$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | 0.0E+0 | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | 0.0E+0 | 0.0E+0 | 0.0E+0 | 0.0E+0 | 0.0E+0 | 0.0E+0 | $\begin{aligned} & \hline 0.0 \mathrm{E}+ \\ & 0 \\ & \hline \end{aligned}$ | 0.0E+0 | $0.0 \mathrm{E}+0$ |
| $\begin{aligned} & \hline \text { EC } \\ & 29 \\ & \hline \end{aligned}$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ | 0.0E+0 | 0.0E+0 | 0.0E+0 | $\begin{aligned} & \hline 0.0 \mathrm{E}+ \\ & 0 \\ & \hline \end{aligned}$ | $0.0 \mathrm{E}+0$ | $0.0 \mathrm{E}+0$ |

TABLE XII. STATISTICAL COMPARISON OF ỌMOA AND STATE-OF-THE-ART ALGORITHMS FOR CEC 2017, 50D

| Tag | JADE | SHADE | UMOEAsII | MVMO | LSHADE-cnEpSin | EBOwithCMAR | OMOA |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| EC 1 | $\begin{aligned} & \text { 5.2385E-14 (2.5180E- } \\ & 14) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 0.0000 \mathrm{E}+00 \\ & (0.0000 \mathrm{E}+00) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 0.0000 \mathrm{E}+00 \\ & (0.0000 \mathrm{E}+00) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.3313 \mathrm{E}-05(5.6019 \mathrm{E}- \\ & 06) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 0.0000 \mathrm{E}+00 \\ & (0.0000 \mathrm{E}+00) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.00+00(0.00+00) \\ & + \end{aligned}$ | $\begin{aligned} & 2.80 \mathrm{E}+05 \\ & (6.00 \mathrm{E}+04) \end{aligned}$ |
| EC 2 | $\begin{aligned} & 1.3112 \mathrm{E}+13 \\ & (8.5354 \mathrm{E}+13) \end{aligned}$ | $\begin{aligned} & 1.0801 \mathrm{E}+12 \\ & (4.3906 \mathrm{E}+12) \end{aligned}$ | $\begin{aligned} & 0.0000 \mathrm{E}+00 \\ & (0.0000 \mathrm{E}+00) \end{aligned}$ | $\begin{aligned} & \hline 1.8060 \mathrm{E}+17 \\ & (1.2778 \mathrm{E}+18) \end{aligned}$ | $\begin{aligned} & 1.5686 \mathrm{E}+00 \\ & (1.9314 \mathrm{E}+00) \end{aligned}$ | $\begin{aligned} & 0.00+00(0.00+00) \\ & + \end{aligned}$ | $\begin{aligned} & 2.20 \mathrm{E}+05 \\ & (3.60 \mathrm{E}+04) \end{aligned}$ |
| EC 3 | $\begin{aligned} & \hline 1.7712 \mathrm{E}+04 \\ & (3.7017 \mathrm{E}+04) \\ & + \end{aligned}$ | $\begin{aligned} & \hline 0.0000 \mathrm{E}+00 \\ & (0.0000 \mathrm{E}+00) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { 2.1202E-09 (8.8715E- } \\ & 09) \\ & + \end{aligned}$ | $\begin{aligned} & \text { 5.3095E-07 (1.0965E- } \\ & 07) \\ & + \end{aligned}$ | $\begin{aligned} & \hline 0.0000 \mathrm{E}+00 \\ & (0.0000 \mathrm{E}+00) \\ & + \end{aligned}$ | $\begin{aligned} & 0.00+00(0.00+00) \\ & + \end{aligned}$ | $\begin{aligned} & 3.40 \mathrm{E}+05 \\ & (6.60 \mathrm{E}+04) \end{aligned}$ |
| EC 4 | $\begin{aligned} & 4.9625 \mathrm{E}+01 \\ & (4.7914 \mathrm{E}+01) \end{aligned}$ | $\begin{aligned} & \hline 5.6885 \mathrm{E}+01 \\ & (4.6262 \mathrm{E}+01) \end{aligned}$ | $\begin{aligned} & 6.5462 \mathrm{E}+01 \\ & (5.2164 \mathrm{E}+01) \end{aligned}$ | $\begin{aligned} & \hline 3.5808 \mathrm{E}+01 \\ & (3.6684 \mathrm{E}+01) \end{aligned}$ | $\begin{aligned} & \hline 5.1401 \mathrm{E}+01 \\ & (4.4262 \mathrm{E}+01) \end{aligned}$ | $\begin{aligned} & \hline 4.29 \mathrm{E}+01 \\ & (3.32 \mathrm{E}+0 \mathrm{l}) \end{aligned}$ | $\begin{aligned} & 3.30 \mathrm{E}+01 \\ & (4.80 \mathrm{E}+01) \end{aligned}$ |
| EC 5 | $\begin{aligned} & \hline 5.4288 \mathrm{E}+01 \\ & (8.8034 \mathrm{E}+00) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 3.2859 \mathrm{E}+01 \\ & (5.0387 \mathrm{E}+00) \\ & + \end{aligned}$ | $\begin{aligned} & \hline 5.0801 \mathrm{E}+00 \\ & (1.6684 \mathrm{E}+00) \\ & + \end{aligned}$ | $\begin{aligned} & \hline 8.0787 \mathrm{E}+01 \\ & (1.6432 \mathrm{E}+01) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 2.5166 \mathrm{E}+01 \\ & (6.4447 \mathrm{E}+00) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & 7.58 \mathrm{E}+00 \\ & 2.42 \mathrm{E}+00 \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & 6.60 \mathrm{E}+07 \\ & (0.00 \mathrm{E}+00) \end{aligned}$ |
| EC 6 | $\begin{aligned} & 1.4489 \mathrm{E}-13(9.1172 \mathrm{E}- \\ & 14) \\ & + \end{aligned}$ | $\begin{aligned} & \hline 8.3876 \mathrm{E}-04(1.0169 \mathrm{E}- \\ & 03) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.1951 \mathrm{E}-06(1.9013 \mathrm{E}- \\ & 06) \\ & + \end{aligned}$ | $\begin{aligned} & \text { 5.4321E-03 (3.3038E- } \\ & 03) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 9.1569 \mathrm{E}-07(1.0750 \mathrm{E}- \\ & 06) \\ & + \\ & + \end{aligned}$ | $\begin{aligned} & \hline 8.54 \mathrm{E}-08 \\ & (1.14 \mathrm{E}-07) \\ & + \end{aligned}$ | $\begin{aligned} & 4.00 \mathrm{E}+03 \\ & (3.80 \mathrm{E}+02) \end{aligned}$ |
| EC 7 | $\begin{aligned} & 1.0140 \mathrm{E}+02 \\ & (6.4883 \mathrm{E}+00) \end{aligned}$ | $\begin{aligned} & \hline 8.0964 \mathrm{E}+01 \\ & (3.7800 \mathrm{E}+00) \end{aligned}$ | $5.6459 \mathrm{E}+01(7.1546 \mathrm{E}-$ <br> 01) | $\begin{aligned} & \hline 1.2320 \mathrm{E}+02 \\ & (1.2795 \mathrm{E}+01) \end{aligned}$ | $\begin{aligned} & \hline 7.6639 \mathrm{E}+01 \\ & (6.0618 \mathrm{E}+00) \end{aligned}$ | $\begin{aligned} & \hline 5.79 \mathrm{E}+01 \\ & (1.53 \mathrm{E}+00) \end{aligned}$ | $\begin{aligned} & 0.00 \mathrm{E}+00 \\ & (0.00 \mathrm{E}+00) \end{aligned}$ |
| EC 8 | $\begin{aligned} & \hline 5.5234 \mathrm{E}+01 \\ & (7.7643 \mathrm{E}+00) \end{aligned}$ | $\begin{aligned} & \hline 3.2355 \mathrm{E}+01 \\ & (3.8252 \mathrm{E}+00) \end{aligned}$ | $\begin{aligned} & \hline 4.7781 \mathrm{E}+00 \\ & (1.6264 \mathrm{E}+00) \end{aligned}$ | $\begin{aligned} & \hline 7.5910 \mathrm{E}+01 \\ & (1.6122 \mathrm{E}+01) \end{aligned}$ | $\begin{aligned} & \hline 2.6319 \mathrm{E}+01 \\ & (6.5917 \mathrm{E}+00) \end{aligned}$ | $\begin{aligned} & \hline \text { 7.9IE+00 } \\ & (2.47 \mathrm{E}+00) \end{aligned}$ | $\begin{aligned} & 0.00 \mathrm{E}+00 \\ & (0.00 \mathrm{E}+00) \end{aligned}$ |
| EC 9 | $\begin{aligned} & 1.1773 \mathrm{E}+00 \\ & (1.3141 \mathrm{E}+00) \\ & - \end{aligned}$ | $\begin{aligned} & 1.1123 \mathrm{E}+00(9.3715 \mathrm{E}- \\ & 01) \end{aligned}$ | $\begin{aligned} & 1.7555 \mathrm{E}-03(1.2536 \mathrm{E}- \\ & 02) \end{aligned}$ | $\begin{aligned} & 7.3843 \mathrm{E}+00 \\ & (5.7735 \mathrm{E}+00) \\ & - \end{aligned}$ | $\begin{aligned} & 0.0000 \mathrm{E}+00 \\ & (0.0000 \mathrm{E}+00) \\ & = \end{aligned}$ | $\begin{aligned} & \text { 0.00+00 } \\ & (0.00+00) \\ & = \end{aligned}$ | $\begin{aligned} & 0.00 \mathrm{E}+00 \\ & (0.00 \mathrm{E}+00) \end{aligned}$ |
| $\begin{aligned} & \text { EC } \\ & 10 \end{aligned}$ | $\begin{aligned} & \begin{array}{l} 3.7500 \mathrm{E}+03 \\ (2.5448 \mathrm{E}+02) \\ - \end{array} \end{aligned}$ | $\begin{aligned} & \hline 3.3444 \mathrm{E}+03 \\ & (2.9402 \mathrm{E}+02) \end{aligned}$ | $\begin{aligned} & \hline 3.3804 \mathrm{E}+03 \\ & (4.7255 \mathrm{E}+02) \end{aligned}$ | $\begin{aligned} & \hline 3.4971 \mathrm{E}+03 \\ & (4.3138 \mathrm{E}+02) \end{aligned}$ | $\begin{aligned} & \hline 3.2001 \mathrm{E}+03 \\ & (3.3972 \mathrm{E}+02) \end{aligned}$ | $\begin{aligned} & \hline 3 . \\ & (4.01 \mathrm{E}+02) \end{aligned} 11 \mathrm{E}+03$ | $\begin{aligned} & 0.00 \mathrm{E}+00 \\ & (0.00 \mathrm{E}+00) \end{aligned}$ |
| $\begin{aligned} & \text { EC } \\ & 11 \end{aligned}$ | $\begin{aligned} & \hline 1.3612 \mathrm{E}+02 \\ & (3.3972 \mathrm{E}+01) \\ & - \end{aligned}$ | $\begin{aligned} & \hline 1.2065 \mathrm{E}+02 \\ & (2.9317 \mathrm{E}+01) \end{aligned}$ | $\begin{aligned} & \hline 4.5701 \mathrm{E}+01 \\ & (9.1852 \mathrm{E}+00) \end{aligned}$ | $\begin{aligned} & 4.7488 \mathrm{E}+01 \\ & (8.7237 \mathrm{E}+00) \\ & - \end{aligned}$ | $\begin{aligned} & \hline 2.1393 \mathrm{E}+01 \\ & (2.0902 \mathrm{E}+00) \end{aligned}$ | $\begin{aligned} & \hline 2.64 \mathrm{E}+01 \\ & (3.36 \mathrm{E}+00) \end{aligned}$ | $\begin{aligned} & 0.00 \mathrm{E}+00 \\ & (0.00 \mathrm{E}+00) \end{aligned}$ |
| $\begin{aligned} & \text { EC } \\ & 12 \end{aligned}$ | $\begin{aligned} & \hline 5.1468 \mathrm{E}+03 \\ & (3.3233 \mathrm{E}+03) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 5.1362 \mathrm{E}+03 \\ & (2.8785 \mathrm{E}+03) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 2.1449 \mathrm{E}+03 \\ & (5.3559 \mathrm{E}+02) \\ & + \end{aligned}$ | $\begin{aligned} & \hline 1.2955 \mathrm{E}+03 \\ & (2.7935 \mathrm{E}+02) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 1.4753 \mathrm{E}+03 \\ & (3.6472 \mathrm{E}+02) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.94 \mathrm{E}+03 \\ & (5.34 \mathrm{E}+02) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.20 \mathrm{E}+05 \\ & (1.00 \mathrm{E}+04) \end{aligned}$ |


| $\begin{aligned} & \text { EC } \\ & 13 \end{aligned}$ | $\begin{aligned} & \hline 3.0338 \mathrm{E}+02 \\ & (2.6999 \mathrm{E}+02) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 2.6565 \mathrm{E}+02 \\ & (1.4944 \mathrm{E}+02) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 5.1787 \mathrm{E}+01 \\ & (2.1985 \mathrm{E}+01) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 4.3776 \mathrm{E}+01 \\ & (1.7622 \mathrm{E}+01) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 6.9430 \mathrm{E}+01 \\ & (3.4457 \mathrm{E}+01) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 4.14 \mathrm{E}+01 \\ & (2.45 \mathrm{E}+01) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & 6.90 \mathrm{E}+10 \\ & (1.10 \mathrm{E}+10) \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { EC } \\ & 14 \end{aligned}$ | $\begin{aligned} & 1.0519 \mathrm{E}+04 \\ & (3.1138 \mathrm{E}+04) \end{aligned}$ | $\begin{aligned} & 2.1578 \mathrm{E}+02 \\ & (7.2995 \mathrm{E}+01) \end{aligned}$ | $\begin{aligned} & 2.9299 \mathrm{E}+01 \\ & (2.4831 \mathrm{E}+00) \end{aligned}$ | $\begin{aligned} & 4.8524 \mathrm{E}+01 \\ & (1.2153 \mathrm{E}+01) \end{aligned}$ | $\begin{aligned} & 2.6522 \mathrm{E}+01 \\ & (2.4924 \mathrm{E}+00) \end{aligned}$ | $\begin{aligned} & 3.12 \mathrm{E}+0 \mathrm{I} \\ & (3.52 \mathrm{E}+00) \end{aligned}$ | $\begin{aligned} & 0.00 \mathrm{E}+00 \\ & (0.00 \mathrm{E}+00) \end{aligned}$ |
| $\begin{aligned} & \mathrm{EC} \\ & 15 \end{aligned}$ | $\begin{aligned} & 3.4992 \mathrm{E}+02 \\ & (4.4266 \mathrm{E}+02) \end{aligned}$ | $\begin{aligned} & \hline 3.2262 \mathrm{E}+02 \\ & (1.4201 \mathrm{E}+02) \end{aligned}$ | $\begin{aligned} & \hline 4.1468 \mathrm{E}+01 \\ & (1.0651 \mathrm{E}+01) \end{aligned}$ | $\begin{aligned} & \hline 4.4630 \mathrm{E}+01 \\ & (1.1280 \mathrm{E}+01) \end{aligned}$ | $\begin{aligned} & 2.5596 \mathrm{E}+01 \\ & (4.0567 \mathrm{E}+00) \end{aligned}$ | $\begin{aligned} & 2.94 \mathrm{E}+0 \mathrm{I} \\ & (5.20 \mathrm{E}+00) \end{aligned}$ | $\begin{aligned} & 0.00 \mathrm{E}+00 \\ & (0.00 \mathrm{E}+00) \end{aligned}$ |
| $\begin{aligned} & \mathrm{EC} \\ & 16 \end{aligned}$ | $\begin{aligned} & 8.5696 \mathrm{E}+02 \\ & (1.7532 \mathrm{E}+02) \end{aligned}$ | $\begin{aligned} & 7.3389 \mathrm{E}+02 \\ & (1.8854 \mathrm{E}+02) \end{aligned}$ | $\begin{aligned} & \hline 3.9288 \mathrm{E}+02 \\ & (1.5514 \mathrm{E}+02) \end{aligned}$ | $\begin{aligned} & 8.4082 \mathrm{E}+02 \\ & (1.9349 \mathrm{E}+02) \end{aligned}$ | $\begin{aligned} & 2.7453 \mathrm{E}+02 \\ & (9.9692 \mathrm{E}+01) \end{aligned}$ | $\begin{aligned} & \hline 3.46 \mathrm{E}+02 \\ & (1.46 \mathrm{E}+02) \end{aligned}$ | $\begin{aligned} & 0.00 \mathrm{E}+00 \\ & (0.00 \mathrm{E}+00) \end{aligned}$ |
| $\begin{aligned} & \mathrm{EC} \\ & 17 \end{aligned}$ | $\begin{aligned} & \hline 6.0010 \mathrm{E}+02 \\ & (1.2128 \mathrm{E}+02) \end{aligned}$ | $\begin{aligned} & \hline 5.1634 \mathrm{E}+02 \\ & (1.1109 \mathrm{E}+02) \end{aligned}$ | $\begin{aligned} & \hline 3.1356 \mathrm{E}+02 \\ & (1.0636 \mathrm{E}+02) \end{aligned}$ | $\begin{aligned} & \hline 5.1999 \mathrm{E}+02 \\ & (1.3382 \mathrm{E}+02) \end{aligned}$ | $\begin{aligned} & \hline 2.0706 \mathrm{E}+02 \\ & (7.3064 \mathrm{E}+01) \end{aligned}$ | $\begin{aligned} & \hline 2.75 \mathrm{E}+02 \\ & (5.63 \mathrm{E}+0 \mathrm{I}) \end{aligned}$ | $\begin{aligned} & 0.00 \mathrm{E}+00 \\ & (0.00 \mathrm{E}+00) \end{aligned}$ |
| $\begin{aligned} & \text { EC } \\ & 18 \end{aligned}$ | $\begin{aligned} & 1.8906 \mathrm{E}+02 \\ & (1.2561 \mathrm{E}+02) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.8946 \mathrm{E}+02 \\ & (1.0338 \mathrm{E}+02) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline \mathbf{3 . 5 9 9 7 E}+01 \\ & (8.7118 \mathrm{E}+00) \\ & + \end{aligned}$ | $\begin{aligned} & \hline 4.1756 \mathrm{E}+01 \\ & (1.9445 \mathrm{E}+01) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 2.4332 \mathrm{E}+01 \\ & (2.1179 \mathrm{E}+00) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 3.20 \mathrm{E}+01 \\ & (5.99 \mathrm{E}+00) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.20 \mathrm{E}+05 \\ & (1.00 \mathrm{E}+04) \end{aligned}$ |
| $\begin{aligned} & \mathrm{EC} \\ & 19 \end{aligned}$ | $\begin{aligned} & 3.2429 \mathrm{E}+02 \\ & (1.2561 \mathrm{E}+03) \end{aligned}$ | $\begin{aligned} & 1.5976 \mathrm{E}+02 \\ & (5.6842 \mathrm{E}+01) \\ & - \\ & \hline \end{aligned}$ | $\begin{aligned} & 2.2807 \mathrm{E}+01 \\ & (3.7669 \mathrm{E}+00) \\ & - \end{aligned}$ | $\begin{aligned} & 1.7338 \mathrm{E}+01 \\ & (5.1321 \mathrm{E}+00) \\ & -\quad \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 1.7406 \mathrm{E}+01 \\ & (2.4713 \mathrm{E}+00) \\ & -\quad \\ & \hline \end{aligned}$ | $\begin{aligned} & 2.45 \mathrm{E}+0 \mathrm{I} \\ & (3.94 \mathrm{E}+00) \end{aligned}$ | $\begin{aligned} & 0.00 \mathrm{E}+00 \\ & (0.00 \mathrm{E}+00) \end{aligned}$ |
| $\begin{aligned} & \text { EC } \\ & 20 \end{aligned}$ | $\begin{aligned} & \hline 4.3806 \mathrm{E}+02 \\ & (1.3382 \mathrm{E}+02) \end{aligned}$ | $\begin{aligned} & \hline 3.3382 \mathrm{E}+02 \\ & (1.2079 \mathrm{E}+02) \end{aligned}$ | $\begin{aligned} & \hline 2.3041 \mathrm{E}+02 \\ & (1.2312 \mathrm{E}+02) \end{aligned}$ | $\begin{aligned} & 3.2965 \mathrm{E}+02 \\ & (1.4772 \mathrm{E}+02) \end{aligned}$ | $\begin{aligned} & \hline 1.1412 \mathrm{E}+02 \\ & (3.5483 \mathrm{E}+01) \end{aligned}$ | $\begin{aligned} & \hline 1.47 \mathrm{E}+02 \\ & (7.44 \mathrm{E}+01) \end{aligned}$ | $\begin{aligned} & 0.00 \mathrm{E}+00 \\ & (0.00 \mathrm{E}+00) \end{aligned}$ |
| $\begin{aligned} & \text { EC } \\ & 21 \end{aligned}$ | $\begin{aligned} & 2.5198 \mathrm{E}+02 \\ & (9.6384 \mathrm{E}+00) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & 2.3338 \mathrm{E}+02 \\ & (5.1139 \mathrm{E}+00) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 2.0681 \mathrm{E}+02 \\ & (2.5498 \mathrm{E}+00) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 2.7719 \mathrm{E}+02 \\ & (1.6036 \mathrm{E}+01) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { 2.2676E+02 } \\ & (7.0598 \mathrm{E}+00) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 2.111 \mathrm{E}+02 \\ & (4.06 \mathrm{E}+00) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & 4.30 \mathrm{E}+05 \\ & (3.40 \mathrm{E}+04) \end{aligned}$ |
| $\begin{aligned} & \mathrm{EC} \\ & 22 \end{aligned}$ | $\begin{aligned} & 3.3364 \mathrm{E}+03 \\ & (1.8053 \mathrm{E}+03) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 3.1774 \mathrm{E}+03 \\ & (1.5566 \mathrm{E}+03) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.7929 \mathrm{E}+03 \\ & (1.9112 \mathrm{E}+03) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 3.2653 \mathrm{E}+03 \\ & (1.7185 \mathrm{E}+03) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.5950 \mathrm{E}+03 \\ & (1.6659 \mathrm{E}+03) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 3.65 \mathrm{E}+02 \\ & (9.24 \mathrm{E}+02) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & 9.20 \mathrm{E}+11 \\ & (1.70 \mathrm{E}+11) \end{aligned}$ |
| $\begin{aligned} & \text { EC } \\ & 23 \end{aligned}$ | $\begin{aligned} & 4.7956 \mathrm{E}+02 \\ & (1.1766 \mathrm{E}+01) \end{aligned}$ | $\begin{aligned} & 4.5916 \mathrm{E}+02 \\ & (8.7508 \mathrm{E}+00) \end{aligned}$ | $\begin{aligned} & 4.3459 \mathrm{E}+02 \\ & (5.2143 \mathrm{E}+00) \end{aligned}$ | $\begin{aligned} & 5.0490 \mathrm{E}+02 \\ & (1.5646 \mathrm{E}+01) \end{aligned}$ | $\begin{aligned} & 4.3929 \mathrm{E}+02 \\ & (6.9001 \mathrm{E}+00) \end{aligned}$ | $\begin{aligned} & 4.34 \mathrm{E}+02 \\ & 8.16 \mathrm{E}+00 \end{aligned}$ | $\begin{aligned} & 0.00 \mathrm{E}+00 \\ & (0.00 \mathrm{E}+00) \end{aligned}$ |
| $\begin{aligned} & \mathrm{EC} \\ & 24 \end{aligned}$ | $\begin{aligned} & 5.4197 \mathrm{E}+02 \\ & (7.6206 \mathrm{E}+00) \end{aligned}$ | $\begin{aligned} & \hline 5.3106 \mathrm{E}+02 \\ & (7.4577 \mathrm{E}+00) \end{aligned}$ | $\begin{aligned} & 5.0810 \mathrm{E}+02 \\ & (2.6001 \mathrm{E}+00) \end{aligned}$ | $\begin{aligned} & \hline 5.8374 \mathrm{E}+02 \\ & (1.6940 \mathrm{E}+01) \end{aligned}$ | $\begin{aligned} & 5.1282 \mathrm{E}+02 \\ & (5.5948 \mathrm{E}+00) \end{aligned}$ | $\begin{aligned} & \hline 5.06 \mathrm{E}+02 \\ & (3.85 \mathrm{E}+00) \end{aligned}$ | $\begin{aligned} & 0.00 \mathrm{E}+00 \\ & (0.00 \mathrm{E}+00) \end{aligned}$ |
| $\begin{aligned} & \text { EC } \\ & 25 \end{aligned}$ | $\begin{aligned} & 5.1923 \mathrm{E}+02 \\ & (3.4820 \mathrm{E}+01) \end{aligned}$ | $\begin{aligned} & \hline 5.0694 \mathrm{E}+02 \\ & (3.6446 \mathrm{E}+01) \end{aligned}$ | $\begin{aligned} & 4.8281 \mathrm{E}+02 \\ & (6.4445 \mathrm{E}+00) \end{aligned}$ | $\begin{aligned} & 5.0912 \mathrm{E}+02 \\ & (3.1226 \mathrm{E}+01) \end{aligned}$ | $\begin{aligned} & \hline 4.8034 \mathrm{E}+02 \\ & (1.0816 \mathrm{E}+00) \end{aligned}$ | $\begin{aligned} & \hline 4.89 \mathrm{E}+02 \\ & (2.47 \mathrm{E}+01) \end{aligned}$ | $\begin{aligned} & 0.00 \mathrm{E}+00 \\ & (0.00 \mathrm{E}+00) \end{aligned}$ |
| $\begin{aligned} & \mathrm{EC} \\ & 26 \end{aligned}$ | $\begin{aligned} & 1.6146 \mathrm{E}+03 \\ & (1.2169 \mathrm{E}+02) \end{aligned}$ | $\begin{aligned} & 1.4168 \mathrm{E}+03 \\ & (9.7281 \mathrm{E}+01) \end{aligned}$ | $\begin{aligned} & 5.7211 \mathrm{E}+02 \\ & (4.0709 \mathrm{E}+02) \end{aligned}$ | $\begin{aligned} & 1.9319 \mathrm{E}+03 \\ & (2.8632 \mathrm{E}+02) \end{aligned}$ | $\begin{aligned} & 1.2026 \mathrm{E}+03 \\ & (1.1870 \mathrm{E}+02) \end{aligned}$ | $\begin{aligned} & 7.06 \mathrm{E}+02 \\ & (4.06 \mathrm{E}+02) \end{aligned}$ | $\begin{aligned} & 0.00 \mathrm{E}+00 \\ & (0.00 \mathrm{E}+00) \end{aligned}$ |
| F27 | $\begin{aligned} & 5.5080 \mathrm{E}+02 \\ & (2.3427 \mathrm{E}+01) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 5.4925 \mathrm{E}+02 \\ & (2.7842 \mathrm{E}+01) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 5.3743 \mathrm{E}+02 \\ & (1.7376 \mathrm{E}+01) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 5.4355 \mathrm{E}+02 \\ & (1.7557 \mathrm{E}+01) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & 5.2543 \mathrm{E}+02 \\ & (9.2143 \mathrm{E}+00) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & 5.22 \mathrm{E}+02 \\ & (7.75 \mathrm{E}+00) \\ & + \\ & \hline \end{aligned}$ | $\begin{aligned} & 4.30 \mathrm{E}+05 \\ & (3.40 \mathrm{E}+04) \end{aligned}$ |
| $\begin{aligned} & \text { EC } \\ & 28 \end{aligned}$ | $\begin{aligned} & \hline 4.9185 \mathrm{E}+02 \\ & (2.0882 \mathrm{E}+01) \\ & - \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 4.7943 \mathrm{E}+02 \\ & (2.4173 \mathrm{E}+01) \\ & - \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 4.7289 \mathrm{E}+02 \\ & (2.1643 \mathrm{E}+01) \\ & - \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { 4.6481E+02 } \\ & (1.5047 \mathrm{E}+01) \\ & - \\ & \hline \end{aligned}$ | $\begin{aligned} & 4.5913 \mathrm{E}+02 \\ & (1.1904 \mathrm{E}+01) \end{aligned}$ | $\begin{aligned} & \hline 4.67 \mathrm{E}+02 \\ & (1.79 \mathrm{E}+0 \mathrm{I}) \end{aligned}$ | $\begin{aligned} & 0.00 \mathrm{E}+00 \\ & (0.00 \mathrm{E}+00) \end{aligned}$ |
| $\begin{aligned} & \mathrm{EC} \\ & 29 \end{aligned}$ | $\begin{aligned} & \hline 4.7761 \mathrm{E}+02 \\ & (8.0661 \mathrm{E}+01) \end{aligned}$ | $\begin{aligned} & \hline 4.8716 \mathrm{E}+02 \\ & (1.0502 \mathrm{E}+02) \end{aligned}$ | $\begin{aligned} & \hline 3.6326 \mathrm{E}+02 \\ & (2.0650 \mathrm{E}+01) \end{aligned}$ | $\begin{aligned} & 4.8938 \mathrm{E}+02 \\ & (1.1489 \mathrm{E}+02) \end{aligned}$ | $\begin{aligned} & \hline 3.5289 \mathrm{E}+02 \\ & (9.7796 \mathrm{E}+00) \end{aligned}$ | $\begin{aligned} & \hline 3.47 \mathrm{E}+02 \\ & (1.97 \mathrm{E}+0 \mathrm{I}) \end{aligned}$ | $\begin{aligned} & \mathbf{0 . 0 0 E}+00 \\ & (0.00 \mathrm{E}+00) \end{aligned}$ |
| $w / t / l$ | 10/0/19 | 10/0/19 | 11/0/18 | 9/0/20 | 11/1/17 | 11/1/17 |  |

TABLE XIII. Time Complexity Analysis

| Time Complexity | T1 | T2 | TO | $(\mathbf{a v T 2}$ - T1)/T0 |
| :--- | :--- | :--- | :--- | :--- |
| 10D | 0.164781 | 0.556989 | $6.80 \mathrm{E}-02$ | $5.77 \mathrm{E}+00$ |
| 30D | 0.1695 | 0.627578 | $6.80 \mathrm{E}-02$ | $6.74 \mathrm{E}+00$ |
| 50D | 0.18455 | 0.715318 | $6.80 \mathrm{E}-02$ | $7.81 \mathrm{E}+00$ |
| 100D | 0.24258 | 0.846715 | $6.80 \mathrm{E}-02$ | $8.89 \mathrm{E}+00$ |

## K. Comparison of OMOA with the Winners of CEC2017 (EC1-EC29)

The subsection presents a performance comparison between the 50D problem size for OMOA and other state-ofart high-performing algorithms, especially those that won the CEC2017 competition for real-parameter single objective optimization challenges, as shown in Table XII. The last row represents the values of a Wilcoxon rank-sum test at an alpha value of 0.05 . The terms designate the status of the OMOA
against each competing algorithm such that $w(+$. .mean..win) $/ t(=$..mean.tie) $/ l(-.$. mean.loss $)$ For an algorithm making its first entry, the results show very high success [41] shown by Table XII; OMOA had remarkably shown better performance on most of the complex problems considered, as the last row shows. Also, OMOA showed better performances compared with the winners of the competition (competing method, equity, OMOA $\rightarrow$ w/t/l), e.g., (EBOwithCMAR won 11, equal in 1 and OMOA won 17).

## L. Benchmark Design Real Engineering CEC 2020 Single Objective Problems

Eight (8) difficult engineering design-constrained problems that exhibit functional inequality and equality constraints are considered; compared with state-of-the-art algorithms from CEC 2020 real-world optimization issues presented in [42-44]. Among the results presented are the experiments' statistical best, mean, median, worst, and standard deviations. Generally, all models follow a structure as shown in Eq. (15).
$\min f(x)$

$$
\begin{equation*}
\text { s.t. : } g_{n}(x) \leq 0, n=1, \ldots, m \tag{11}
\end{equation*}
$$

Where f is the fitness, xs ' are the design variables, g is the constraint with less than equality (often greater than for maximization problems), and n is the number of constraints. The conversion of the functional constraint from inequality to equality transforms the problem into equation (16).

$$
\begin{gather*}
f_{p}(x)=f(x)+o \sum_{n=1}^{m} \Phi_{n}\left[g_{n}(x)\right]^{2} \\
\text { s.t. } \quad o>0(\text { i.e.penalty factor }) \\
1 \text { if } g_{n} \text { is violated } \\
\Phi_{n}=\begin{array}{l}
\text { if } g_{n} \text { is satisfied }
\end{array} \tag{12}
\end{gather*}
$$

Where $f_{p(x)}$ is the penalized objective function. Highperforming state-of-the-art algorithms are adopted and compared against the design of certain engineering problems of Fig. 18 (a: Welded beam), (b: Pressure Vessel, and c: Compression Spring). The constraint violations are considered, and the penalty function method is used, which often transforms a constrained problem into an unconstrained continuous counterpart for ease of implementation.


Fig. 18. Engineering design parameter problems.

## M. Statistical Comparison of Results for Tension / Compression Spring Design Problem

The design problem in Fig 18 (c) aims at reducing the weight of the tension/compression spring without compromising domain properties like the shear stress, frequency wave, and displacement functionalities [45]. The control variables are wire diameter (x1), mean coil diameter (x2), and the number of coils (x3); the mathematical formulation is detailed in [42]. Upon the experiment, OMOA yielded the most optimal weight compared to the other highperforming algorithms within a minimal number of function evaluations. The result of the compared simulation is shown in Table XIV.

## N. Statistical Comparison of the Results for Welded Beam Problem

The welded beam problem Fig. 18 (b) [46] is to minimize the cost of construction. The impacting constraints include shear $\operatorname{stress}(\tau)$; bending stress in the beam $(\sigma)$; buckling load
of the bar $\left(\mathrm{P}_{\mathrm{c}}\right)$; end deflection of the beam $(\delta)$ and side constraints. The decision variables are (1) the thickness of the weld (x1), the length of the attached part of bar (x2), the height of the bar (x3) and the thickness of the bar (x4). The model formulation is given in [42]. And compared simulated statistical results in Table XV with parametric results in Table XVI.

TABLE XIV. RESULTS FOR THE TENSION / COMPRESSION SPRING DESIGN PROBLEM

| Method | Worst | Mean | Best | SD | NFEs |
| :--- | :--- | :--- | :--- | :--- | :--- |
| GA1 | 0,012822 | 0.012769 | 0.012704 | $3.94 \mathrm{E}-05$ | 900,000 |
| GA2 | 0.012973 | 0.012742 | 0.012681 | $5.90 \mathrm{E}-05$ | 80000 |
| CAEP | 0.015116 | 0.013568 | 0.012721 | $8.42 \mathrm{E}-04$ | 50,020 |
| CPSO | 0.012924 | 0.012924 | 0.012674 | $5.20 \mathrm{E}-04$ | 240,000 |
| HPSO | 0.012719 | 0.012707 | 0.012665 | $1.58 \mathrm{E}-05$ | 81,000 |
| NM-PSO | 0.012633 | 0.012631 | 0.01263 | $8.47 \mathrm{E}-07$ | 80,000 |
| G-QPSO | 0.017759 | 0.013524 | 0.012665 | 0.001268 | 2000 |
| QPSO | 0.018127 | 0.013854 | 0.012669 | 0.001341 | 2000 |
| PSO | 0.071802 | 0.019555 | 0.012857 | 0.011662 | 2000 |
| DE | 0.01279 | 0.012703 | 0.01267 | $2.7 \mathrm{E}-05$ | 204,800 |
| DELC | 0.012665 | 0.012665 | 0.012665 | $1.3 \mathrm{E}-07$ | 20,000 |
| DEDS | 0.012738 | 0.012669 | 0.012665 | $1.3 \mathrm{E}-05$ | 24,000 |
| HEAA | 0.012665 | 0.012665 | 0.012665 | $1.4 \mathrm{E}-09$ | 24,000 |
| PSO-DE | 0.012665 | 0.012665 | 0.012665 | $1.2 \mathrm{E}-08$ | 24,950 |
| SC | 0.016717 | 0.012922 | 0.012669 | $5.9 \mathrm{E}-04$ | 25,167 |
| $(\mu+\lambda)-$ ES | NA | 0.013165 | 0.012689 | $3.9 \mathrm{E}-04$ | 30,000 |
| ABC | NA | 0.012709 | 0.012665 | $1.28 \mathrm{E}-02$ | 30,000 |
| LCA | 0.01266667 | 0.0126654 | 0.0126652 | $3.88 \mathrm{E}-07$ | 15,000 |
| WCA | 0.012952 | 0.012746 | 0.012665 | $8.06 \mathrm{E}-05$ | 11,750 |
| IGMM | 0.0135125 | 0.0128657 | 0.0126652 | $2.56 \mathrm{E}-04$ | 4000 |
| APSO | 0.014937 | 0.013297 | 0.0127 | $6.85 \mathrm{E}-04$ | 120,000 |
| MCEO | 0.01350901 | 0.0127196 | 0.0126605 | $3.79 \mathrm{E}-05$ | 2000 |
| OMOA | $\mathbf{0 . 0 1 1 6 0}$ | $\mathbf{0 . 0 1 1 2 4 1}$ | $\mathbf{0 . 0 1 1 1 0 9 0}$ | $\mathbf{0 . 0 0 0 2 3 5 4}$ | $\mathbf{2 0 0 0}$ |

TABLE XV. Statistical Results for Welded Beam Problem

| Method | Worst | Mean | Best | SD | NFEs |
| :--- | :--- | :--- | :--- | :--- | :--- |
| CAEP | 3.179709 | 1.971809 | 1.724852 | 0.443 | 50,020 |
| CPSO | 1.782143 | 1.748831 | 1.7314849 | 0.0129 | 240,000 |
| HPSO | 1.814295 | 1.74904 | 1.724852 | 0.0401 | 81,000 |
| PSO-DE | 1.724852 | 1.724852 | 1.724852 | $6.7 \mathrm{E}-16$ | 66,600 |
| NM-PSO | 1.733393 | 1.726373 | 1.72472 | 0.0035 | 80,000 |
| SC | 6.399678 | 3.002588 | 2.385434 | 0.96 | 33,095 |
| DE | 1.824105 | 1.768158 | 1.733461 | 0.0221 | 204,800 |
| WCA | 1.744697 | 1.726427 | 1.724856 | 0.00429 | 46,450 |
| LCA | 1.7248523 | 1.7248523 | 1.7248523 | $7.11 \mathrm{E}-15$ | 15,000 |
| IGMM | 1.74769 | 1.732152 | 1.724855 | $7.14 \mathrm{E}-03$ | 8000 |
| APSO | 1.993999 | 1.877851 | 1.736193 | 0.076118 | 50,000 |
| MCEO | 1.7248732 | 1.7248621 | 1.7248523 | $1.02 \mathrm{E}-05$ | 12,500 |
| OMOA | $\mathbf{1 . 6 7 6 4 5 7 7}$ | $\mathbf{1 . 6 2 2 5 9 5}$ | $\mathbf{1 . 3 5 3 4 5 4 9}$ | $\mathbf{0 . 2 3 9 0 7 7 3}$ | $\mathbf{6 0 0 0 0}$ |

TABLE XVI. COMPARISONS OF THE BEST SOLUTIONS FOR WELDED BEAM

| DV | CAEP | HGA | NM-PSO | WCA | IGMM | MCEO | OMOA |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $x 1$ | 0.2057 | 0.2057 | 0.20583 | 0.205728 | 0.205729 | 0.2057296 | 0.15203 |
| $x 2$ | 3.4705 | 3.4705 | 3.468338 | 3.470522 | 3.470496 | 3.4704887 | 8.02626 |
| $x 3$ | 9.0366 | 9.0366 | 9.036624 | 9.03662 | 9.036625 | 9.0366239 | 6.08668 |
| $x 4$ | 0.2057 | 0.2057 | 0.20573 | 0.205729 | 0.205730 | 0.2057296 | 0.15775 |
| $\mathrm{g} 1(x)$ | -769.34 | -769.34 | -770.3698 | -0.034128 | -771.187 | -771.2021 | $-0.3760+\mathrm{E} 4$ |
| $\mathrm{g} 2(x)$ | 4.48154 | 4.48154 | -0.053122 | $-3.49 \mathrm{E}-05$ | -0.05976 | $-2.88 \mathrm{E}-05$ | -1.83846+E4 |
| $\mathrm{g} 3(x)$ | -0.2283 | $-0.2283$ | $-0.228310$ | $-1.19 \mathrm{e}-6$ | $-0.228310$ | -0.228310 | -0.00002+E4 |
| $\mathrm{g} 4(x)$ | 0 | 0 | $1.00 E-04$ | -3.43298 | $-1 \mathrm{e}-6$ | 0 | 0 |
| $\mathrm{g} 5(x)$ | 2.60337 | 2.603347 | -0.031555 | -0.080728 | -0.0319920 | $-1.85 \mathrm{E}-05$ | -0.0222+E4 |
| $\mathrm{g} 6(x)$ | -0.0807 | -0.08070 | -0.080830 | -0.23554 | -0.08072 | -0.08073 | 0 |
| $\mathrm{g} 7(x)$ | -3.4332 | -3.43321 | -3.43316 | -0.013503 | -3.4329802 | -3.43298 | -0.0003+E4 |
| $f(x)$ | 1.72457 | 1.724577 | 1.724720 | 1.724856 | 1.7248552 | 1.724852 | 1.622595 |

In less than 60000 functional evaluations of 10 runs, OMOA yielded a mean cost that is the most optimal for the welded beam in comparison while obeying the constraints.

## O. Results for Pressure Vessel Design Problem

The Pressure Vessel Design objective in Fig. 18 (b) [47] is to minimize the cost associated with materials, building, and welding of a cylindrical vessel with capped ends and a hemispherical-shaped head. The impacting variables include the shell thickness $x(1)$, the head thickness $x(2)$, the inner radius $x(3)$, and the length of the cylindrical section excluding the head $x(4)$; the model formulation is given in [42].

The yield of OMOA on the Pressure Vessel design problem produced the best optimal mean value and had a far smaller number of function evaluations of Table XVII.

OMOA met all the inequality constraints; best mean fitness as shown, followed by MCEO, WCA, and NM-PSO, respectively. However, contrary to the large number assigned to the penalty using the other algorithms, OMOA found better results with negligible penalty value for problems of spring and welding beam, and even no penalty was applied to vessel design.

TABLE XVII. the Pressure Vessel Design Problem Results

| Method | Worst | Mean | Best | SD | NFEs |
| :--- | :--- | :--- | :--- | :--- | :--- |
| GA1 | 6308.497 | 6293.8432 | 6288.7445 | 7.4133 | 900,000 |
| GA2 | 6469.322 | 6177.2533 | 6059.9463 | 130.9297 | 80,000 |
| CPSO | 6363.8041 | 6147.1332 | 6061.0777 | 86.45 | 240,000 |
| HPSO | 6288.677 | 6099.9323 | 6059.7143 | 86.2 | 81,000 |
| NM-PSO | 5960.0557 | 5946.7901 | 5930.3137 | 9.161 | 80,000 |
| G-QPSO | 7544.4925 | 6440.3786 | 6059.7208 | 448.4711 | 8000 |
| QPSO | 8017.2816 | 6440.3786 | 6059.7209 | 479.2671 | 8000 |
| PSO | 14076.324 | 8756.6803 | 6693.7212 | 1492.567 | 8000 |
| CDE | 6371.0455 | 6085.2303 | 6059.734 | 43.013 | 204,800 |
| WCA | 6590.2129 | 6198.6172 | 5885.3327 | 213.049 | 27,500 |
| LCA | 6090.6114 | 6070.5884 | 6059.8553 | 11.37534 | 24,000 |
| IGMM | 6061.2868 | 6060.1598 | 6059.7143 | 0.5421 | 8000 |
| APSO | 7544.49272 | 6470.71568 | 6059.7242 | 326.9688 | 200,000 |
| MCEO | 6060.3096 | 6060.0315 | 6059.7143 | 1.2532 | 7500 |
| OMOA | $\mathbf{8 7 0 . 8 9 8 3}$ | $\mathbf{8 4 8 . 7 3 3 3}$ | $\mathbf{8 4 6 . 2 7 0 5 5}$ | $\mathbf{7 . 7 8 8 0 0 5 2}$ | $\mathbf{2 0 0 0}$ |

## P. Robot Gripper Problem

The complexity involved in manipulating the grippers to minimize the difference between the minimum and maximum forces of the robotic action is ongoing research. Seven design variables, geometric properties, with about seven inequality constraints, are targeted. The Mathematical formulations are found here in [48].


Fig. 19. Schematics of robotics gripper system.
Fig. 19 is schematics of the robotic gripper system, and the experimental result is shown in Table XVIII.

TABLE XVIII. THE Statistical Results of Robotic Gripper Optimizations

| Variables | (TLBO) | AOS | OMOA |
| :--- | :--- | :--- | :--- |
| Best | 4.247643634 | 2.54383686 | $\mathbf{0 . 0 0 0 0 0 0 0 0 0 0}$ |
| Mean | 4.93770095 | 2.791745357 | $\mathbf{0 . 6 6 6 1 7 6 5 8 6 9}$ |
| Worst | 8.141973 | 3.14335667 | 6.4675702717 |
| Std-Dev | 0.56 | 0.226323642 | 1.8645193071 |
| a | 150 | 149.9973899 | 27.248574186 |
| b | 150 | 149.880236 | 150 |
| c | 200 | 200 | 200 |
| d | 0 | 0 | 0 |
| e | 150 | 149.9954554 | 71.18076298 |
| f | 100 | 100.9429469 | 300 |
| t | 2.339539113 | 2.297394124 | 2.124666881 |
| $\mathrm{~g}_{1}(\mathrm{x})$ | -28.09283911 | -49.99996461 | -47.7172 |
| $\mathrm{~g}_{2}(\mathrm{x})$ | -21.90716089 | $-5.23 \mathrm{E}-06$ | -2.2828 |
| $\mathrm{~g}_{3}(\mathrm{x})$ | -33.64959994 | -49.99996461 | -200.6371 |
| $\mathrm{~g}_{4}(\mathrm{x})$ | -16.35040006 | $-3.53 \mathrm{E}-05$ | 150.6371 |
| $\mathrm{~g}_{5}(\mathrm{x})$ | -79999.998 | -79737.112 | 0 |
| $\mathrm{~g}_{6}(\mathrm{x})$ | $-9.8 \mathrm{E}-11$ | -36.02117726 | -4.0000 |
| $\mathrm{~g}_{7}(\mathrm{x})$ | -0.00001 | -0.943046876 | -0.0200 |

The experimental result of OMOA on the gripper problem showcases a new optimum as against the optimum global set value [42]; also better than the competing algorithms in comparison [44].

## Q. Rolling Element Bearing

Five design variables that affect the optimal design of a rolling bearing with the capacity to carry load efficiently amidst nine inequality constraints are considered in the design. The mathematical derivations are provided by [42], while we show the schematics in Fig. 20.


Fig. 20. Schematics of rolling bearing.
The result of the experiment is shown in Table XIX.

TABLE XIX. Results of Rolling Bearing and Statistic Comparisons wITH OMOA

|  | (TLBO) | ABC | GWO | ALO | AOS | OMOA |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Best | 81859.74 | $\begin{aligned} & 85428.24 \\ & 95 \\ & \hline \end{aligned}$ | $\begin{aligned} & 85529.08 \\ & 30 \end{aligned}$ | $\begin{aligned} & 85546.63 \\ & 77 \\ & \hline \end{aligned}$ | $\begin{aligned} & 83918.492 \\ & 93 \end{aligned}$ | $\begin{aligned} & \hline 6232.0171 \\ & 29 \\ & \hline \end{aligned}$ |
| $\begin{aligned} & \hline \text { Mea } \\ & \mathrm{n} \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 81438.98 \\ & 7 \\ & \hline \end{aligned}$ | $\begin{aligned} & 85121.75 \\ & 44 \end{aligned}$ | $\begin{aligned} & 83395.08 \\ & 49 \\ & \hline \end{aligned}$ | $\begin{aligned} & 84032.86 \\ & 36 \end{aligned}$ | $\begin{aligned} & 82175.212 \\ & 66 \\ & \hline \end{aligned}$ | $\begin{aligned} & 9468.3133 \\ & 94 \end{aligned}$ |
| Wor <br> st | $80807.85$ | $\begin{aligned} & 83859.08 \\ & 51 \\ & \hline \end{aligned}$ | $\begin{aligned} & 43543.45 \\ & 08 \\ & \hline \end{aligned}$ | $\begin{aligned} & 73872.81 \\ & 64 \\ & \hline \end{aligned}$ | $\begin{aligned} & 83826.383 \\ & 37 \\ & \hline \end{aligned}$ | $\begin{aligned} & 14246.414 \\ & 60 \\ & \hline \end{aligned}$ |
| $\begin{aligned} & \text { Std- } \\ & \text { Dev } \\ & \hline \end{aligned}$ | 0.66 | 362.57 | 8224.5 | 3121.8 | 23.38511 | $\begin{aligned} & 2239.4436 \\ & 27 \end{aligned}$ |
| $\mathrm{D}_{\mathrm{m}}$ | 21.42559 | 125.6599 | 125.7090 | 125.718 | 125 | 150 |
| $\mathrm{D}_{\mathrm{b}}$ | 125.7191 | 21.40862 | 21.42316 | $\begin{aligned} & 21.42524 \\ & 2 \end{aligned}$ | 21.875 | $\begin{aligned} & 10.860427 \\ & 72 \\ & \hline \end{aligned}$ |
| Z | 11 | 11 | 11 | 11 | $\begin{aligned} & 10.777009 \\ & 05 \\ & \hline \end{aligned}$ | $\begin{aligned} & 4.5100000 \\ & 00 \\ & \hline \end{aligned}$ |
| $\mathrm{f}_{\mathrm{i}}$ | 0.515 | 0.515 | 0.515 | 0.515 | 0.515 | $\begin{aligned} & 0.5942954 \\ & 10 \\ & \hline \end{aligned}$ |
| $\mathrm{f}_{0}$ | 0.515 | 0.515 | 0.529322 | $\begin{aligned} & \hline 0.515170 \\ & 18 \\ & \hline \end{aligned}$ | 0.515 | $\begin{aligned} & 0.5802317 \\ & 89 \\ & \hline \end{aligned}$ |
| $\mathrm{K}_{\mathrm{Dmi}}$ | 0.424266 | 0.427166 | 0.420867 | $\begin{aligned} & 0,454164 \\ & 6 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.4761106 \\ & 18 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.4000000 \\ & 00 \\ & \hline \end{aligned}$ |
| $\mathrm{K}_{\mathrm{Dma}}$ | 0.633948 | 0.668849 | 0.633296 | $\begin{aligned} & 0.646492 \\ & 4 \end{aligned}$ | $\begin{aligned} & 0.6581426 \\ & 45 \end{aligned}$ | $\begin{aligned} & \text { 0.6000000 } \\ & 00 \end{aligned}$ |
| E | 0.3 | 0.3 | 0.300224 | $\begin{aligned} & 0.300001 \\ & 22 \\ & \hline \end{aligned}$ | 0.3 | $\begin{aligned} & 0.3000000 \\ & 00 \end{aligned}$ |
| e | 0.068858 | 0.071386 | 0.02 | $\begin{aligned} & 0.063800 \\ & 3 \\ & \hline \end{aligned}$ | 0.02 | $\begin{aligned} & 0.0200000 \\ & 00 \\ & \hline \end{aligned}$ |
| Chi | 0.799498 | 0.6 | 0.619432 | $\begin{aligned} & 0.610759 \\ & 2 \end{aligned}$ | $\begin{aligned} & \hline 0.6182422 \\ & 02 \end{aligned}$ | $\begin{aligned} & \hline 0.6000000 \\ & 00 \end{aligned}$ |

With an optimum global set at (25287.918415), the experimental result of Table XIX shows that OMOA had set a better global optimum as it also performed better than the competing algorithms [44].

## R. Gas Transmission Compressor Design (GTCD)

Four variables with one inequality constraint are targeted when designing the gas transmission compressor. The work [42] provides the mathematical formulation while we show the schematics in Fig. 21 and the solutions provided by many optimization state-of-the-art to designs.


Fig. 21. Schematic of gas transmission compressor system with design variables.

The results of the comparison for the experiment on GTCD are shown in Table XX.

TABLE XX. Results of Optimization of GTCD and Statistical OUTCOMES

| Algorithms |  |  |  | Optimum <br> cost |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  | x 1 | x 2 | x 3 | x 4 |  |
| CLPSO | 45.8830 | 1.571778 | 27.18201 | 1.45592 | $3.7381430 \mathrm{E}+06$ |
| ABC | 50.0000 | 1.185882 | 24.89145 | 0.39507 | $2.9845610 \mathrm{E}+06$ |
| ACOR | 49.6067 | 1.174456 | 23.92940 | 0.37862 | $2.9671090 \mathrm{E}+06$ |
| ABC | 50.0000 | 1.207839 | 24.49319 | 0.45792 | $2.9755610 \mathrm{E}+06$ |
| KH | 35.6206 | 1.092393 | 31.99460 | 1.10937 | $3.4608480 \mathrm{E}+06$ |
| WOA | 49.7095 | 1.178115 | 24.72718 | 0.38796 | $2.9650350 \mathrm{E}+06$ |
| HHO | 49.9844 | 1.180801 | 24.20547 | 0.39429 | $2.9650910 \mathrm{E}+06$ |
| BOA | 20.0000 | 1.000000 | 20.00000 | 0.16475 | $3.1364520 \mathrm{E}+06$ |
| HGSO | 50.0000 | 1.164785 | 25.72731 | 0.35606 | $2.9689110 \mathrm{E}+06$ |
| LIACOR | 50.0000 | 1.178480 | 24.58628 | 0.38882 | $2.9648960 \mathrm{E}+06$ |
| SMO | 50.0000 | 1.178284 | 24.59259 | 0.38835 | $2.9648954 \mathrm{E}+06$ |
| OMOA | 50.0000 | 1.00000 | 20.1422 | 60 | $\mathbf{9 . 8 0 8 1 9 1 1 5}$ |

The experimental results show OMOA had a set a new global optimum than that set by the competition as the global optimum is $(2.9648954173 \mathrm{E}+06)$ [42], with the other algorithms as presented in [49].

## S. Himmelblau's Function

This nonlinear function has been used to test many novel metaheuristic algorithms; it has five main design variables and six inequality constraints to be handled, as shown in Himmelblau [50]. In Table XXI, we show the results of the performances of the metaheuristic algorithms used in comparison.

The experimental result shows that OMOA obtained a better minimum compared to the competing algorithms and set a new global optimum compared to the global presented by [42], which is $-3.066554 \mathrm{E}+04$, with the other algorithms as presented in [49].

## T. Multiple Disk Clutch Brake Design Problem

The design objective is to minimize the mass of the multiple disk clutch brake, five decision variables with nine nonlinear constraints. The mathematical formulation is given in [42].

TABLE XXI. Statistical and Performance of Algorithms on the Himmelblau Complex Problem

| $\begin{gathered} \hline \text { Algorith } \\ \mathrm{m} \end{gathered}$ | X1 | X2 | X3 |  | X4 | $\begin{gathered} \hline \text { OPTIMA } \\ \text { L } \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| CLPSO | 86.3511 | 34.276 | 31.279 |  | 32.758 | $-2.99 \mathrm{E}+04$ |
| ABC | 78 | $\begin{aligned} & \hline 33.272 \\ & 9 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 30.6521 \\ & 6 \end{aligned}$ | $\begin{aligned} & \hline 44.3040 \\ & 2 \end{aligned}$ | 36.4902 | $-3.05 \mathrm{E}+04$ |
| ACOR | 78 | 33 | $\begin{aligned} & 30.0480 \\ & 8 \\ & \hline \end{aligned}$ | $\begin{aligned} & 44.9380 \\ & 6 \\ & \hline \end{aligned}$ | 36.7053 | -3.06E+04 |
| ABC | 78 | 33 | $\begin{aligned} & 30.1961 \\ & 7 \end{aligned}$ | 45 | 36.3524 | -3.06E+04 |
| KH | $\begin{aligned} & 78.9989 \\ & 2 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 33.005 \\ & 7 \\ & \hline \end{aligned}$ | $\begin{aligned} & 30.6702 \\ & 1 \\ & \hline \end{aligned}$ | $\begin{aligned} & 43.6357 \\ & 9 \\ & \hline \end{aligned}$ | 35.5313 | -3.04E+04 |
| WOA | $\begin{aligned} & 79.3603 \\ & 1 \\ & \hline \end{aligned}$ | 33 | $\begin{aligned} & 30.0490 \\ & 6 \\ & \hline \end{aligned}$ | $\begin{aligned} & 42.5411 \\ & 0 \\ & \hline \end{aligned}$ | 37.2748 | -3.05E+04 |
| HHO | 78 | 33 | $\begin{aligned} & 30.0075 \\ & 7 \\ & \hline \end{aligned}$ | $\begin{aligned} & 44.9929 \\ & 7 \\ & \hline \end{aligned}$ | 36.7473 | -3.06E+04 |
| BOA | 78 | 33 | $\begin{aligned} & 30.3113 \\ & 9 \\ & \hline \end{aligned}$ | $\begin{aligned} & 39.5904 \\ & 9 \\ & \hline \end{aligned}$ | 31.5837 | -3.01E+04 |
| HGSO | 78 | 33 | $\begin{aligned} & 3.10983 \\ & 1 \\ & \hline \end{aligned}$ | $\begin{aligned} & 4.00229 \\ & 9 \end{aligned}$ | 3.62353 | -3.03E+04 |
| $\begin{aligned} & \hline \text { LIACO } \\ & \text { R } \\ & \hline \end{aligned}$ | 78 | 33 | $\begin{aligned} & 29.9952 \\ & 6 \\ & \hline \end{aligned}$ | $\begin{aligned} & 45.0000 \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & 36.7758 \\ & 1 \\ & \hline \end{aligned}$ | $-3.06 \mathrm{E}+04$ |
| SMO | 78 | 33 | 29.995 |  | 36.7758 | $-3.06 \mathrm{E}+04$ |
| OMOA | 79.8729 | 43.856 | 27.078 | 29.1039 | 29.1039 | -3.19E+04 |



Fig. 22. The schematic geometric representation of the multiple disc clutch design.

Fig. 22 is schematics geometric representation of the clutch disc problem. However, the experimental results are shown in Table XXII.

TABLE XXII. Shows the Results of the Performance of Metaheuristic Methods on the Clutch Design Problem

| $\begin{gathered} \text { Algorith } \\ \text { ms } \\ \hline \end{gathered}$ | x1 | x2 | x3 | x4 | x5 | optimum |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| CLPSO | $\begin{aligned} & \hline 75.959 \\ & 32 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 97.069 \\ & 36 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.0105 \\ & 8 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 909.478 \\ & 64 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 2.0972 \\ & 3 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 0.280152637613 \\ & 733 \\ & \hline \end{aligned}$ |
| ABC | $\begin{aligned} & 69.999 \\ & 74 \\ & \hline \end{aligned}$ | $\begin{aligned} & 90.000 \\ & 00 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.0000 \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & 697.479 \\ & 83 \\ & \hline \end{aligned}$ | $\begin{aligned} & 2.0000 \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.235242474598 \\ & 156 \\ & \hline \end{aligned}$ |
| ACOR | $\begin{aligned} & \hline 70.000 \\ & 00 \end{aligned}$ | $\begin{aligned} & 90.000 \\ & 00 \end{aligned}$ | $\begin{aligned} & 1.0000 \\ & 0 \end{aligned}$ | $\begin{aligned} & 718.003 \\ & 97 \end{aligned}$ | $\begin{aligned} & \hline 2.0000 \\ & 0 \end{aligned}$ | $\begin{aligned} & \hline 0.235242457900 \\ & 804 \\ & \hline \end{aligned}$ |
| ABC | $\begin{aligned} & 70.000 \\ & 00 \\ & \hline \end{aligned}$ | $\begin{aligned} & 90.000 \\ & 00 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.0000 \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & 317.170 \\ & 55 \\ & \hline \end{aligned}$ | $\begin{aligned} & 2.0000 \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 0.235242457900 \\ & 804 \\ & \hline \end{aligned}$ |
| KH | $\begin{aligned} & 70.000 \\ & 00 \\ & \hline \end{aligned}$ | $\begin{aligned} & 90.000 \\ & 00 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.0000 \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & 481.079 \\ & 88 \\ & \hline \end{aligned}$ | $\begin{aligned} & 2.0000 \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.235242458886 \\ & 112 \\ & \hline \end{aligned}$ |
| WOA | $\begin{aligned} & 70.000 \\ & 00 \\ & \hline \end{aligned}$ | $\begin{aligned} & 90.000 \\ & 00 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.0000 \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & 182.355 \\ & 43 \\ & \hline \end{aligned}$ | $\begin{aligned} & 2.0000 \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 0.235242457901 \\ & 052 \\ & \hline \end{aligned}$ |
| HHO | $\begin{aligned} & 70.000 \\ & 00 \\ & \hline \end{aligned}$ | $\begin{aligned} & 90.000 \\ & 00 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.0000 \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & 304.207 \\ & 38 \\ & \hline \end{aligned}$ | $\begin{aligned} & 2.0000 \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.235242457900 \\ & 804 \\ & \hline \end{aligned}$ |
| BOA | $\begin{aligned} & \hline 67.726 \\ & 99 \\ & \hline \end{aligned}$ | $\begin{aligned} & 90.000 \\ & 00 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.0000 \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 673.069 \\ & 21 \\ & \hline \end{aligned}$ | $\begin{aligned} & 2.0000 \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 0.248171278270 \\ & 212 \\ & \hline \end{aligned}$ |
| HGSO | $\begin{aligned} & 69.999 \\ & 45 \\ & \hline \end{aligned}$ | $\begin{aligned} & 90.000 \\ & 00 \end{aligned}$ | $\begin{aligned} & 1.0000 \\ & 0 \\ & \hline \end{aligned}$ | 8.73600 | $\begin{aligned} & 2.0000 \\ & 0 \end{aligned}$ | $\begin{aligned} & \hline 0.235248138956 \\ & 563 \\ & \hline \end{aligned}$ |
| LIACOR | $\begin{aligned} & 70.000 \\ & 00 \\ & \hline \end{aligned}$ | $\begin{aligned} & 90.000 \\ & 00 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.0000 \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & 169.998 \\ & 45 \end{aligned}$ | $\begin{aligned} & 2.0000 \\ & 0 \end{aligned}$ | $\begin{aligned} & 0.235242457900 \\ & 804 \end{aligned}$ |
| SMO | 70.000 | 90.000 | 1.000 | 999.99 | 2.000 | 0.2352424579 |
| OMOA | 80.000 | 90.005 | 1.000 | 1000.0 | 2.000 | 0.1250434142 |

OMOA performed better than ABC , which was reported as best at the time of competition report, and others in this design problem and further set a much better global optimum than benchmarked in [42]; 0.23524245790; with the other algorithms as presented in [49].

## IV. CONCLUSION

In this work, Odigbo Metaheuristic Optimization Algorithm - OMOA, a new nature-inspired population-based metaphor, was proposed and used in experiments and engineering designs with very great performance. The idea stemmed from the informal learning pattern and discipleship, which is ingrained in the socio-cultural behavior of the indigenous peoples - the Ndigbo of a West African tribe is presented. The learners cope through practice and observation. The experiment conducted considered 30 benchmark unconstraint problems, 29 CEC 2017 (50D) real-parameter single objective constraint optimization, and about 8 engineering design constrained problems from CEC 2020; the results showed that OMOA had balanced exploitation and exploratory capacities with very good convergence time too. Comparison to the performance of other well-established state-of-the-art algorithms depicts the exceptional performance of the automata. The significant test also confirms the relative efficiency of OMOA with t -values and p -values presented in Table VIII and summarized in Table IX. The convergence time test using the Rastrigin function also shows OMOA had better speed than the contender in Table X. The competing algorithms were the most award winners in past competitions from 2017 till date. In all complex engineering problems presented, OMOA had performed remarkably well and had, in some cases, set new minimum attainable best solutions; Of interest are the new values better than the set global optimums in some functions and engineering designs (Clutch Disc, Himmelblau, GTCD, Rolling Bearing, Robotic Gripper).

The future direction is to further validate with the most recent CECs and design optimization problems in other fields. Meanwhile, OMOA shows merit to be considered in the current state-of-the-art.

## ACKNOWLEDGMENT

Akowuah E. K.: Lead Supervision, Validation, Revising the manuscript, providing suggestions, and Feedback on the methodology. Kponyo J. J.: Supervision, Revising the manuscript, Providing suggestions, and Feedback on the methodology. Boateng K. O.: Supervision, Providing Feedback on the approach.

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